

SINGLE STAGE EXPERIMENTAL EVALUATION
OF
SLOTTED ROTOR AND STATOR BLADING

PART VIII - DATA AND PERFORMANCE
FOR SLOTTED STATOR 3

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ABSTRACT

A single stage investigation of a slotted stator was conducted as part of an overall program to evaluate the effect of slots on the performance of highly loaded compressor rotor and stator blade rows. A lightly loaded flow generation rotor was used to provide stator inlet flow. The stator vanes were 65-series airfoils having a calculated diffusion factor based on the turning for an unslotted vane of 0.704, and an inlet Mach number of 0.644 at a radial position 90% of the span from the vane tip. The measured stator total pressure losses were considerably higher than the predicted losses at all radial stations.

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SECTION I
SUMMARY

A single-stage investigation of a slotted stator was conducted as part of an overall program to evaluate the effect of slots on the performance of highly loaded compressor rotor and stator blade rows. The single-stage rig had a hub/tip ratio of 0.8 and a tip diameter of approximately 40 in. The stator vanes were 65-series airfoils having a calculated D-factor of 0.704 based on the turning for an unslotted vane and an inlet Mach number of 0.644 at a radial station 90% of the span from the tip. The vanes had a constant chord length of 2.18 in., an aspect ratio of 1.663, and solidity of 1.099 at the mean radius. The vanes were slotted at approximately 55% chord; the slots extended from 5 to 95% span in each vane. A lightly loaded flow generation rotor was used to provide stator inlet conditions.

The measured D-factor near the stator root was 0.53 at design incidence. The stator deviation angles exceeded the values predicted for design incidence by 9 deg near the root, 1 deg at the mean radius, and 6 deg near the tip. Measured loss coefficient values were considerably larger than the predicted values at all radial stations.

SECTION II
INTRODUCTION

Pratt & Whitney Aircraft is engaged in a program under NASA Contract NAS3-7603 to investigate the application of slots to axial flow compressor rotors and stators. A systematic investigation was conducted to establish the feasibility and extent to which slotted blade concepts can be used to increase allowable blade loadings and the stable operating range of compressor stages. To accomplish this objective, three stator vane rows and three rotor blade rows representing a progression in design diffusion factors were built for test. In the stator tests, a representative state-of-the-art rotor was used to generate the stator inlet flow.

The aerodynamic analysis and design of the test blading and associated hardware were accomplished under the design phase of the program (Reference 1). All rotors and stators were designed with the same rotor exit and stator inlet absolute velocities and air angle distributions to permit testing of any combination of rotor and stator. For design purposes, it was assumed that the flow deviation angle for slotted rotors and stators would be approximately half the values normally used for unslotted blades. As part of the design effort, a series of annular cascade tests with slotted stators was conducted to establish preliminary criteria for the design of rotor and stator slots for the rotating stage test program (Reference 2). The overall and blade element performance data for previously reported slotted blade rows are presented in References 3 through 7.

This report presents the data and performance results obtained with the third slotted stator configuration (Stator 3). Stator 3 blading was designed with 65-series airfoil sections and had calculated design hub values of D-factor loading and inlet Mach number (without slots) of 0.704 and 0.644, respectively. The stator vanes were slotted at approximately 55% chord and the slots extended from 5% to 95% span in each vane. A lightly loaded flow generation rotor was used to establish flow conditions into the test stator. Inlet guide vanes provided rotor prewhirl and exit guide vanes were used to turn the flow back to near-axial.

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Overall performance and blade element data were obtained at 50, 70, 90, 100, and 110% of the design equivalent rotor speed. Blade element data were obtained at 10, 30, 50, 70, and 90% span locations behind each of the three blade rows.

Details of the test equipment, procedures, and test results for the slotted Stator 3 test configuration, as well as pertinent design details, are presented in this report. Complete aerodynamic and mechanical design details are included in Reference 1.

SECTION III
TEST EQUIPMENT

A. FACILITY

The compressor test facility is shown schematically in figure III-1. The compressor rotor is powered by a single-stage turbine using exhaust gases from a J75 slave engine. The turbine speed is regulated by a hydraulically actuated inlet flow control valve. The slave engine exhaust is also used to drive a two-stage exhaust ejector system.

Air entered the compressor test rig through a 103-ft combined inlet duct, plenum, and bellmouth inlet, and exhausted through an exit diffuser to the atmosphere. An area contraction ratio from plenum to compressor inlet of approximately 10:1 provided essentially stagnation conditions in the plenum. The inlet duct and plenum were mounted on a track and could be rolled away from the compressor rig inlet to facilitate configuration changes. The plenum was sealed to the compressor rig inlet section with an inflatable rubber tube seal.

B. COMPRESSOR TEST RIG

The compressor rig, shown in figure III-2, comprises bellmouth inlet, test section, and exhaust section. The test section has a hub/tip ratio of 0.8 and a rotor tip diameter of approximately 40 in. The rotor assembly and shaft are supported on two bearings that transmit loads to the outer case through struts located in the inlet and exhaust case assemblies. The test section has a split outer case that permits guide vane, rotor, and stator assembly changes without removing the rig from the test stand. A set of motor-driven throttle vanes is located in the exhaust case to vary flow rate.

A section view of the flow path is shown in figure III-3. Flow is accelerated through the inlet strut station and guide vanes in a convergent passage to the rotor inlet. Thereafter, the inner wall diameter remains constant at 32.85 in., whereas the outer wall converges further through the rotor blade and stator vane rows to a diameter of 40 in. In general, the flow path is designed to simulate the middle-stage environment of a state-of-the-art multistage compressor.

Provisions were made for end-wall bleed at the rotor tip and stator root and tip, as shown in figure III-4. Bleed air flowed through perforated plate shrouds, shroud manifolds, and 24 approximately equally spaced tubes to individual main collector manifolds for the rotor and stator. The collector manifolds exhausted through the facilities ejector system. Rotor and stator bleed flow rates were controlled and measured separately.

C. STAGE BLADING DESIGN

To expedite this research program, the aerodynamic and mechanical design of the blading was completed and fabrication initiated prior to the completion of the annular cascade program. Final slot configurations were based on the results of the cascade tests. The design details for the inlet guide vane, flow generation rotor, and slotted Stator 3 are given in Reference 1. Pertinent design information is given below for convenience.

1. Inlet Guide Vane

The inlet guide vanes were designed to provide a rotor prewhirl distribution of 38.2 deg at the hub (90% span) to 39.8 deg at the tip (10% span). NACA 63-series blade sections were chosen for this purpose. Details of the guide vane design are presented in table III-1.

2. Flow Generation Rotor

NACA 65-series blade sections were selected for the flow generation rotor blading. The blading was designed with a camber distribution of 36.8 deg at the hub (90% span) to 34.5 deg at the tip (10% span) and with a tip D-factor of 0.379. Details of the rotor design are presented in table III-1.

3. Stator 3

a. Blade Design

Slotted Stator 3 blading was designed with a constant equivalent circular arc camber of 58.34 deg and a constant blade-chord angle of 34.1 deg. The stators are 65-series airfoil sections with a design root (90% span) D-factor of 0.704 (unslotted) and a design inlet Mach number of 0.644.

Table III-1. Geometry Design Data

INLET GUIDE VANE							FLOW GENERATION ROTOR							STATOR 3							Airfoil Series: No. of Blades: Aspect Ratio:	63 50 1.530	Airfoil Series: No. of Blades: Aspect Ratio:	65 60 1.707	Airfoil Series: No. of Blades: Aspect Ratio:	65 58 1.663
Percent Span (from Tip)	κ_0	κ_1	ϕ	γ°	c	σ	t/c	δ°	Percent Span (from Tip)	κ'_1	κ'_2	ϕ	γ°	i_m	0/0*	c	σ	t/c	δ°	$\bar{\omega}'$	Airfoil Series: No. of Blades: Aspect Ratio:	63 50 1.530	Airfoil Series: No. of Blades: Aspect Ratio:	65 60 1.707	Airfoil Series: No. of Blades: Aspect Ratio:	65 58 1.663
90	-26.50	42.10	-68.60	24.70	2.560	1.212	0.060	3.86	90	31.44	-5.38	36.82	13.11	-1.26	1.449	2.210	1.250	0.075	8.54	0.051	Airfoil Series: No. of Blades: Aspect Ratio:	63 50 1.530	Airfoil Series: No. of Blades: Aspect Ratio:	65 60 1.707	Airfoil Series: No. of Blades: Aspect Ratio:	65 58 1.663
50	-27.30	43.70	-71.00	25.50	2.560	1.109	0.060	4.65	50	39.23	2.16	37.07	20.55	-2.20	1.468	2.210	1.149	0.059	8.37	0.045						
10	-28.10	45.30	-73.40	26.30	2.560	1.021	0.060	5.51	10	45.36	10.87	34.49	27.85	-2.60	1.476	2.210	1.071	0.044	8.74	0.045						

Solidity, thickness ratios, and aspect ratios for the selected series airfoils were representative of the middle stage of a state-of-the-art compressor. Additional details of the Stator 3 design are presented in table III-1.

b. Slot Design

Stator 3 slot geometry and location were based on the results of preliminary annular cascade tests of slotted stator vanes and an analysis of Stator 3 suction surface boundary layer separation (References 1 and 2).

The selected slot geometry was similar to a preferred slot geometry determined in the annular cascade program. Blade thickness at the intersection of slot centerline and blade meanline was selected as an approximate scaling parameter to scale the slot size from the oversize (6.5 in. chord) annular cascade vanes to the 2.18-in. chord Stator 3 vanes.

The slot centerline intersected the blade suction surface at 55% chord, approximately halfway between the minimum pressure point and the calculated separation point. This slot location was determined under the annular cascade tests to be superior to an alternative location near the separation point. A schematic drawing and pertinent dimensions of the blade slot are presented in figure III-5. Figure III-6 is a photograph of a slotted Stator 3 vane.

D. INSTRUMENTATION

Instrumentation was provided for overall and blade element performance measurements for each blade row. Axial locations of instrumentation stations are indicated in figure III-3, and schematics showing the detailed instrumentation at each axial location are presented in figures III-7 through III-10.

1. Rig Inlet Conditions

Weight flow was measured with an ASME standard thin plate orifice located in the inlet duct.

Six static pressure taps and six temperature probes were located in the plenum chamber for measurement of inlet total pressure and temperature.

Six equally spaced static pressure taps were located on both the inner and outer walls upstream of the inlet guide vanes (Station 0). From a rig calibration over a wide range of weight flows, a correlation between these static pressures and weight flow was derived and used to check subsequent weight flow measurements.

2. Station 1 (Guide Vane Exit/Rotor Inlet)

A sectional view of the flow path at Station 1 showing the circumferential and radial locations of instrumentation is presented in figure III-7. Rotor inlet air angle measurements were obtained at two circumferential locations with 20-deg wedge traverse probes. A 20-tube wake traverse probe, aligned approximately with the average guide vane exit air angle, was installed to measure the guide vane wake total pressure distribution. Four static pressure taps were located on both the inner and outer walls. The wedge probes and static pressure taps were located approximately along extensions of guide vane midchannel lines. Total and static pressure data were available from the 20-deg wedge probe for comparison.

3. Station 2 (Rotor Exit/Stator Inlet)

A sectional view of the flow path showing the circumferential and radial locations of instrumentation at Station 2 is presented in figure III-8. Two 20-deg wedge traverse probes were used for air angle, total pressure, and total temperature measurements. Three sets of Kiel head total pressure probes were located at radial positions corresponding to 10, 30, 50, and 70% span and two Kiel probes were located at 90% span. The probes were circumferentially located so that the three probes at any given radial position averaged approximately the pressures across a guide vane wake. Four static pressure taps were located on both the inner and outer walls. An 8-deg wedge traverse probe was used for radial static pressure measurements.

4. Station 2A (Stator Exit)

A sectional view of the flow path showing circumferential and radial locations of instrumentation at Station 2A is presented in figure III-9. Stator exit air angle was measured with a 20-deg wedge traverse probe. A 20-tube rake traverse probe was used for measurement of stator vane wake total pressure distribution. Four static pressure taps were located on both the inner and outer walls, and an 8-deg wedge traverse probe was provided for radial static pressure measurement. An internal leak was discovered in the 20-deg wedge probe used at Station 2A introducing an error in probe air angle measurements. Measurements from this probe were therefore not used.

5. Station 3

Station 3 is one chord-length farther from the stator exit plane than Station 2A. Instrumentation at this station (figure III-10) included two 20-deg wedge traverse probes, four sets of Kiel head total pressure probes at 10, 30, 50, 70, and 90% span locations, four sets of Kiel head temperature probes at the same five span locations, and four static pressure taps on both the inner and outer walls. The 20-deg wedge probes were used for stator exit air angle measurements. Stage exit total temperature was based on Kiel head probe temperature measurements at Station 3. Data obtained from the other instrumentation at this station were generally used for comparison with the Station 2A data.

6. Description of Probes

Details of the 20- and 8-deg wedge probes, wake probes, and Kiel pressure and temperature probes are shown in figure III-11. The 20-deg wedge probe senses air angle, total pressure, and total temperature. The 8- and 20-deg wedge probes and the Kiel temperature probes were calibrated for Mach number effect appropriately on probe measurements of static pressure and total temperature.

The wake probes contained 20 total pressure pickups formed by 0.042-in. OD hypo tubing and spaced as shown in the figure.

7. Instrumentation Readout

Traverse probe data (total pressure, static pressure, air angle, total temperature, and radial travel) were recorded on magnetic tape at the rate of 60 samples (2.5 in. probe travel) per minute. Steady-state pressure measurements were obtained using a scannivalve multi-channel pressure transducer system, which includes automatic data recording on IBM cards. Kiel probe temperatures were indicated on a precision potentiometer, and manually recorded.

Plenum pressures, two OD static pressures at Station 0, primary and bleed system flow-measuring-orifice pressures, and two Station 3 midspan Kiel probe pressures were recorded on manometer tubes in the test stand control room to permit setting the desired flow conditions.

8. Special Instrumentation

a. Rotor Speed

Rotor rpm was measured with an electromagnetic pickup mounted adjacent to a 60-tooth gear on the rotor shaft. Gear tooth passing frequency was displayed as rpm on an Anadex digital readout system. A closed loop control system maintained rotor speed to within approximately $\pm 1\%$.

b. Stress

Five rotor blades and two stator vanes were instrumented with strain gages located as shown in figure III-12 to monitor torsional and bending stresses.

c. Vibration

Displacement pickups were mounted on forward and rear sections of the compressor rig outer case to monitor rig vibration.

d. Bleed Flow Rate

The end-wall bleed flow from the rotor and stator rows was measured by means of standard ASME thin plate orifices located in the bleed manifold exhaust ducts.

SECTION IV
PROCEDURES

A. TEST PROCEDURE

1. Wall Bleed Flow Rate Selection

a. Rotor Bleed

With the compressor operating at design speed, the bleed flow rate was adjusted to ensure that there was no recirculation through the bleed manifold from Station 2 (rotor exit) to Station 1 (rotor inlet). This was accomplished by monitoring the static pressure difference between Station 1 and the bleed manifold and adjusting the bleed valve until the manifold pressure was less than that of Station 1. The maximum bleed flow rate attainable with the bleed system was required to produce the desired results at choke conditions (lowest Station 1 static pressure). The valve setting for this flow rate was not changed at other rotor speed and flow conditions.

b. Stator Bleed

With the rotor OD wall bleed set at the maximum rate the procedure described above was repeated for the stator by monitoring the static pressure difference between Station 2 and the stator bleed manifold. It was also necessary to adjust the stator bleed valve for maximum flow to ensure no recirculation at choke conditions. This valve setting was used throughout the program.

2. Stress Survey

Blade stresses were monitored during rig operation at design speed and during operation into the stall region at all rotor speed conditions.

3. Overall and Blade Element Performance Tests

Overall and blade element performance data were obtained at five rotor speed conditions (50, 70, 90, 100, and 110% of design speed) and at approximately six points per speed line to adequately define stator and stage performance between choke and stall. The near-stall point was determined on the basis of strain gage output and stage exit total pressure indicated on manometers. At each speed and flow set point, the fixed pressure and temperature instrumentation data were recorded

five times, corresponding to five discrete radial locations of the inlet guide vane and stator vane wake probes. Traverse data were usually recorded during the last recording of fixed instrumentation. In this manner, representative average values of flow and pressures could be determined for the time period (approximately 45 min) of data recording at each point.

B. DATA REDUCTION PROCEDURES

1. Preliminary Data Reduction

Data reduction was accomplished in three steps using three computer programs. The first step involved conversion of raw data to engineering units. Traverse data (total pressure, static pressure, total temperature, and air angle), obtained at approximately 0.04-in. increments across the span, were automatically tabulated and plotted.

These data were reviewed to identify and eliminate any obviously questionable data prior to the subsequent data reduction step.

The second data reduction step accomplished the following:

1. Mach number corrections to temperature data
2. Mass average of wake probe data
3. Circumferential arithmetic average of fixed and traverse instrumentation data
4. Correction of all pressure and temperature data to NASA standard day ambient conditions
5. Selection by interpolation of total pressure, static pressure, total temperature, and air angle values at specified radial locations for input to the final data reduction step.

All corrected data were available for further inspection in the printed results from this computer program, which included individual data values as well as averaged quantities. The third step in the data reduction procedure involved calculation of overall and blade element performance parameters, which are defined in the following paragraphs.

2. Parameter Calculation

The following overall and blade element performance parameters were calculated for the analysis of test data and the evaluation of slotted Stator 3 performance. Symbols are defined in Appendix A.

a. Overall Performance

(1) Weight Flow

Weight flow is presented in terms of corrected weight flow, defined as

$$W_{corr} = W\sqrt{\theta/\delta}$$

where

W = actual weight flow

θ = ratio of total temperature (plenum) to NASA standard sea level temperature

δ = ratio of total pressure (plenum) to NASA standard sea level pressure.

Values of corrected weight flow presented in the figures and tables include rotor and stator bleed flow rates. Percentage bleed flow rates for the two blade rows are tabulated separately (table B-1).

(2) Pressure Ratio

Pressure ratios were calculated for the rotor, guide-vane-rotor and guide-vane-rotor-stator blade row combinations. Behind the rotor, fixed Kiel head and traverse probe total pressure data were arithmetically averaged at each span location and the profile thus determined was mass-flow averaged across the span.

Behind the guide vane and stator the wake probe pressures were first mass-flow integrated at each span location, and the resulting average pressures were then mass-flow averaged in the radial direction.

(3) Adiabatic Efficiency

Adiabatic efficiency across the rotor is defined as

$$\eta_{ad} = \frac{\frac{\gamma - 1}{\bar{P}_2}}{\frac{\bar{P}_1}{\frac{\bar{T}_3}{\bar{T}_1} - 1}}$$

where:

\bar{P}_1 = mass averaged pressure behind the guide vane

$$T_1 = 518.7^{\circ}\text{R}$$

\bar{P}_2 = mass averaged pressure behind the rotor

\bar{T}_3 = mass averaged temperature behind the stator.

To obtain adiabatic efficiencies for the guide vane-rotor combination or for the entire stage, appropriate average pressures were used.

b. Blade Element Performance

(1) Diffusion Factor

Diffusion factor for the rotor is defined as

$$D = 1 - \frac{V_2'}{V_1} + \frac{\Delta V_\theta' (1 - 2)}{2\sigma V_1}$$

Diffusion factor for the stator is defined as

$$D = 1 - \frac{V_{2A}}{V_2} + \frac{\Delta V_\theta (2 - 2A)}{2\sigma V_2}$$

(2) Deviation

Rotor blade deviation is defined as

$$\delta_2^o = \beta_2' - \kappa_2'$$

Stator deviation is defined as

$$\delta_{2A}^o = \beta_{2A} - \kappa_{2A}$$

where κ_2' and κ_{2A} are the rotor blade and stator vane trailing edge metal angles based on equivalent circular arc camber lines for the 65-series airfoil.

(3) Incidence Angle

Rotor incidence angle is defined as

$$i_{m1} = \beta_1' - \kappa_1'$$

Stator incidence angle is defined as

$$i_{m2} = \beta_2 - \kappa_2$$

where κ_1 and κ_2 are the rotor blade and stator vane leading edge metal angles based on the equivalent circular arc camber lines for the 65-series airfoil.

(4) Total Pressure Loss Coefficient

Total pressure loss coefficient for the rotor is defined as

$$\bar{\omega}_{(1 - 2)}' = \frac{\bar{P}_1' - P_2'}{\bar{P}_1' - p_1}$$

where (-) refers to mass-averaged wake total pressure.

For the inlet guide vanes, total pressure loss coefficient is defined as

$$\bar{\omega}_{(0 - 1)} = \frac{14.69 - \bar{P}_1}{q_o}$$

where q_o is obtained from isentropic flow relationships using orifice weight flow and the annular area at the guide vane inlet.

Total pressure loss coefficient for the stator is defined as

$$\bar{\omega}_{(2 - 2A)} = \frac{P_2 - \bar{P}_{2A}}{P_2 - p_2}$$

(5) Loss Parameter

Stator total pressure loss is also presented in terms of the loss parameter,

$$\frac{\bar{\omega}_{(2 - 2A)} \cos \beta_3}{2\sigma}$$

SECTION V
RESULTS AND DISCUSSION

Performance of slotted Stator 3 was evaluated on the basis of stage pressure rise and efficiency characteristics as functions of rotative speed and weight flow, as well as of blade element diffusion factor, deviation, and loss coefficient as functions of incidence angle, and of loss parameter as a function of D-factor.

Slotted Stator 3 performance results are compared (1) with predicted unslotted Stator 3 performance and (2) with available NASA rotating cascade performance results. Overall and blade element performance parameter values, bleed flow rates, and blade element vector diagram data for the guide vane, rotor, and stator are tabulated in Appendix B.

A. OVERALL PERFORMANCE

Overall performance for the slotted Stator 3 test configuration is presented in terms of efficiency and pressure ratio versus corrected weight flow, $W\sqrt{\theta}/\delta$, and corrected specific weight flow, $W\sqrt{\theta}/\delta A$, in figures V-1, V-2, and V-3, respectively, for the flow generation rotor, guide vane-rotor and guide vane-rotor-Stator 3 combinations. Each figure contains the performance results obtained at the five test rotor speed conditions. Overall performance and percent bleed flows are tabulated in table B-1.

The pressure rise and efficiency of the flow generation rotor (figure V-1) at design equivalent rotor speed and flow conditions are high compared to the predicted values. The rotor incidence was higher than predicted for design conditions, and rotor deviation angle was lower than predicted. These factors combined to increase the work and flow of the stage. Since the temperature rise of the stage is small (about 30 deg) it is expected that the efficiency data for the rotor will show considerable scatter; this source of error becomes significant as stage pressure and temperature rise decrease. Additional discussion of flow generation rotor performance is presented in Reference 6. Figures V-2 and V-3 indicate a large reduction of stage performance due to Stator 3 losses. The influence of high stator losses on a low-work stage ($P_2/P_1 = 1.1 - 1.2$) is expected to be greater than the influence of stator loss on a stage having a higher work input ($P_2/P_1 = 1.3 - 1.4$).

Therefore, the low value of stage efficiency for these tests is not significant.

A comparison of the measured airflow with the airflow calculated from traverse and fixed probe data is presented in figure V-4. The data relating to rotor discharge flow are within the allowable 5% band. Downstream of the stator, a bias toward high integrated weight flows is noticeable and many of the data points fall outside the 5% band. A detailed examination of the data and reduction procedure has shown that this bias is attributable to the numerical integration used in the calculation. As a part of this integration, the mass-averaged total pressure calculated from the stator wake data is used to generate a radial flow distribution, which is then integrated to determine the total flow. The employment of the mass-averaged total pressure in this calculation leads to erroneously high flows since no accounting is made of the displacement thicknesses of the wakes. The magnitude of this flow difference is dependent upon the size of the wake and thus varies with spanwise location and the configuration of the stator and the stator incidence and Mach number. A numerical example is used as an illustration. A data point from figure V-4 was selected for which a large (10%) difference between integrated and orifice-measured flow was noted. The wake rake data were used to calculate the circumferential and radial distribution of flow without recourse to the use of average quantities. A double integration (area) was then performed to determine the flow. Thus computed, the flow was 84.5 lb/sec, compared with 82.7 lb/sec based on the measured orifice flow with deductions for the wall bleed. This difference, 2.1%, is in keeping with the acceptable deviation.

The mass-averaged pressure ratio was subsequently recomputed for this point to observe the extent to which pressure ratio is also affected by the employment of the mass-averaged total pressure of each radial location behind the stator. The recomputed value of 1.118 was well within the plotting accuracy of the value of 1.116 originally computed. Since the calculation of mass-average pressure ratio utilizes the flow computed from the mass-average total pressure at the various diameters in both the numerator and denominator of the weighting fraction, $\Sigma WP / \Sigma W$, it is to be expected that the effect on pressure ratio would be small.

B. BLADE ELEMENT PERFORMANCE

1. Stator Inlet Conditions

The stator inlet air angle and Mach number distributions for design equivalent rotor speed are presented in figure V-5. The stator was operating within 1 to 2 deg of the indicated design air angle distribution at weight flows of 90.04 and 84.71 lb/sec (near choke flow conditions for the stage). The stator-inlet Mach number at design incidence operation was therefore slightly higher than the design inlet Mach number. Flow generation rotor overturning of about 3 deg accounts for the difference between the design weight flow of 80 lb/sec and the weight flow for which stator design incidence was achieved. As a consequence, the stator was subjected to incidence angles in the stall direction from the minimum loss incidence angle over the stator operating range.

2. Stator Loss Coefficient, Deviation, D-Factor

Slotted Stator 3 loss coefficient, deviation angle, and D-factor at design rotor speed are presented as functions of incidence angle in figures V-6 through V-10. Each figure corresponds to one span location. In general, the losses are extremely large relative to two-dimensional flow losses at all span locations. The large deviation angles at 10, 30, 70, and 90% span and the high loss coefficient values indicate a significant amount of flow separation. The diffusion factor values are correspondingly low relative to the predicted values.

Blade element parameters for all speed lines are combined in figures V-11 through V-15. The deviation and D-factor data form well-defined curves with incidence at each of the five span locations. Deviation values may be biased slightly low since measurements of stator exit flow angle were obtained at Station 3, approximately $1\frac{1}{2}$ chord lengths downstream of the stator blade row. The loss coefficient data scatter is attributed to the inherent inaccuracy of pressure measurements in a separated (nonsteady) flow field.

3. Loss Parameter

Loss parameter, $\bar{\omega}_2 - 2A \cos \beta_3 / 2\sigma$, is presented as a function of D-factor for the blade element data obtained at 90, 100 and 110% design rotor speeds in figures V-16a through V-16c. The NASA correlation curve for NASA 65-series annular cascade minimum loss (reference incidence) data reproduced from Reference 8 is shown for comparison. The slotted Stator 3 data are separated according to 90 and 10% span, 70 and 30% span, and 50% span. Darkened symbols refer to minimum loss points. The measured loss parameter values are considerably higher than the NASA correlation curve values.

SECTION VI
CONCLUDING DISCUSSION

Blade element data at five radial locations and overall performance data were obtained for a single stage comprising slotted Stator 3, a flow generation rotor, and inlet guide vanes. Slotted Stator 3 had a design D-factor of 0.704 at a radial location 90% of span from the tip and a constant equivalent camber angle of 58.3 deg. The stator operated close to its design incidence angle at maximum flow conditions. The loss and deviation angle values were high relative to predicted values at all span locations. Diffusion factor values were correspondingly lower than the predicted values. From these results, it is concluded that flow separation from the suction surface of the stator vanes occurred further upstream than predicted (Reference 1). This may have placed the separation point in close proximity to the slot; this condition was found to be undesirable in the preliminary annular cascade studies (Reference 2). It may be necessary to incorporate additional slots closer to the leading edge of highly cambered (60 deg) airfoil sections.

**SECTION VII
ILLUSTRATIONS**

This section contains the illustrations that have been referenced in the preceding sections.

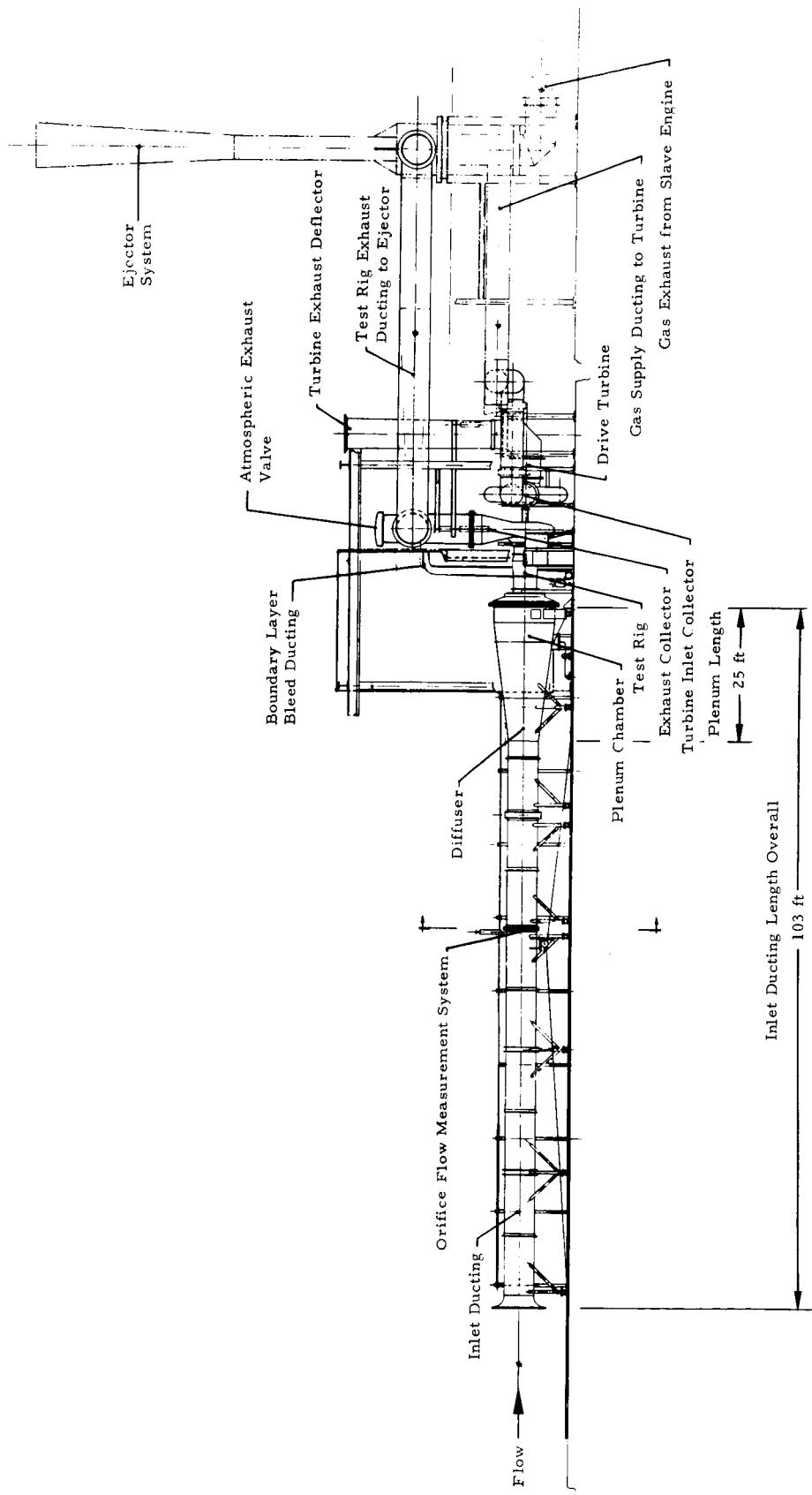
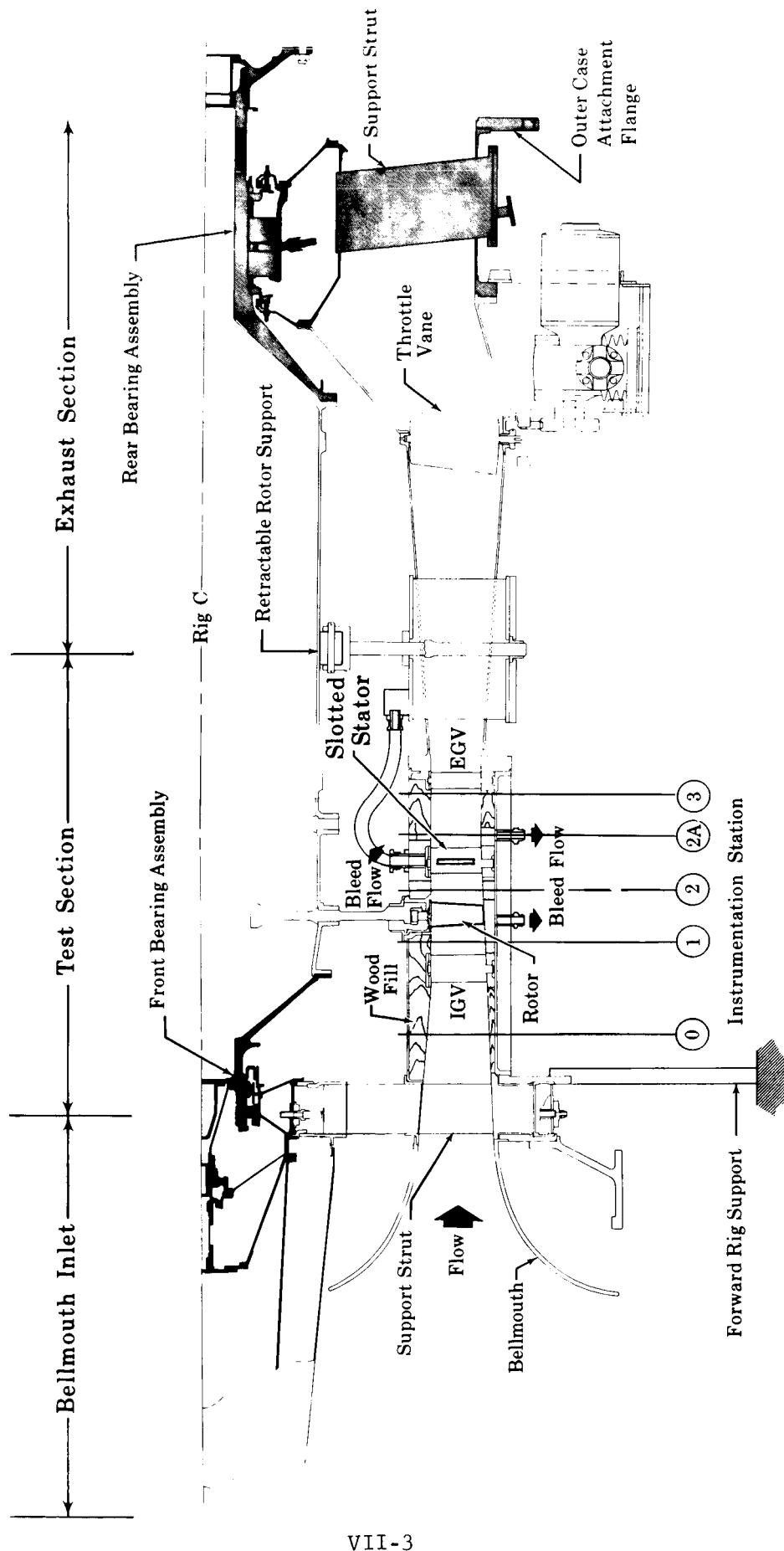


Figure III-1. Compressor Research Facility

FD 10891C



VII-3

Figure III-2. Rotating Axial Flow Cascade Test Rig

FD 14681B

FD 14685A

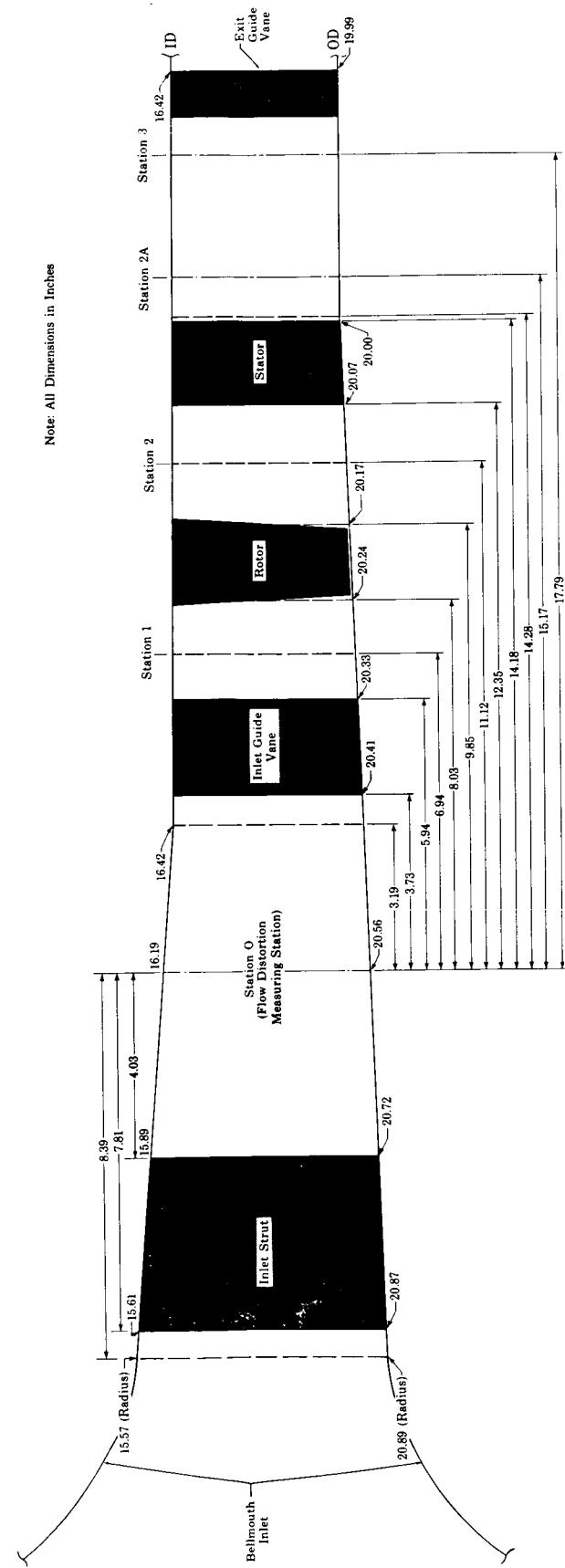


Figure III-3. Flow Path and Instrumentation Stations

Rig E

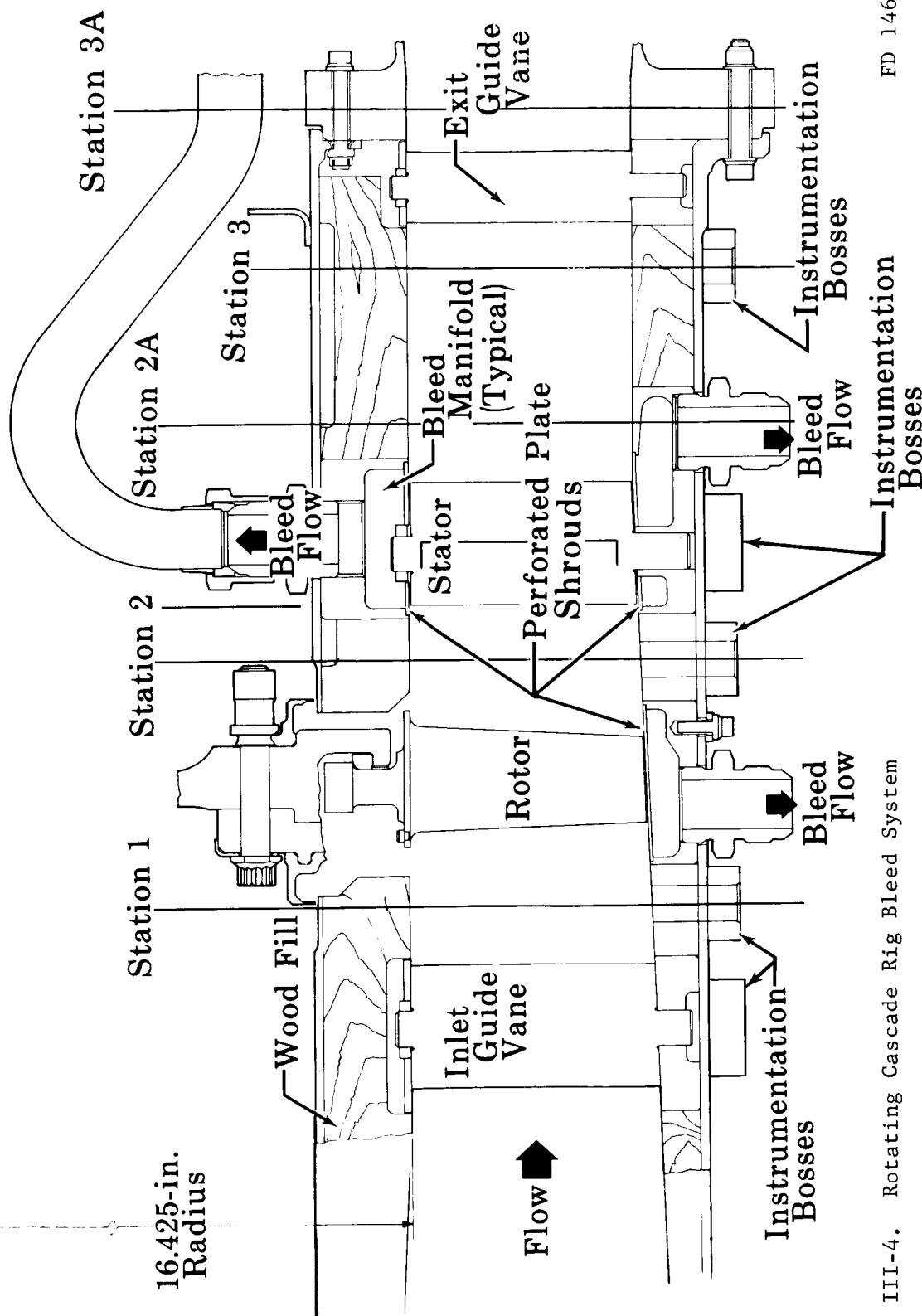
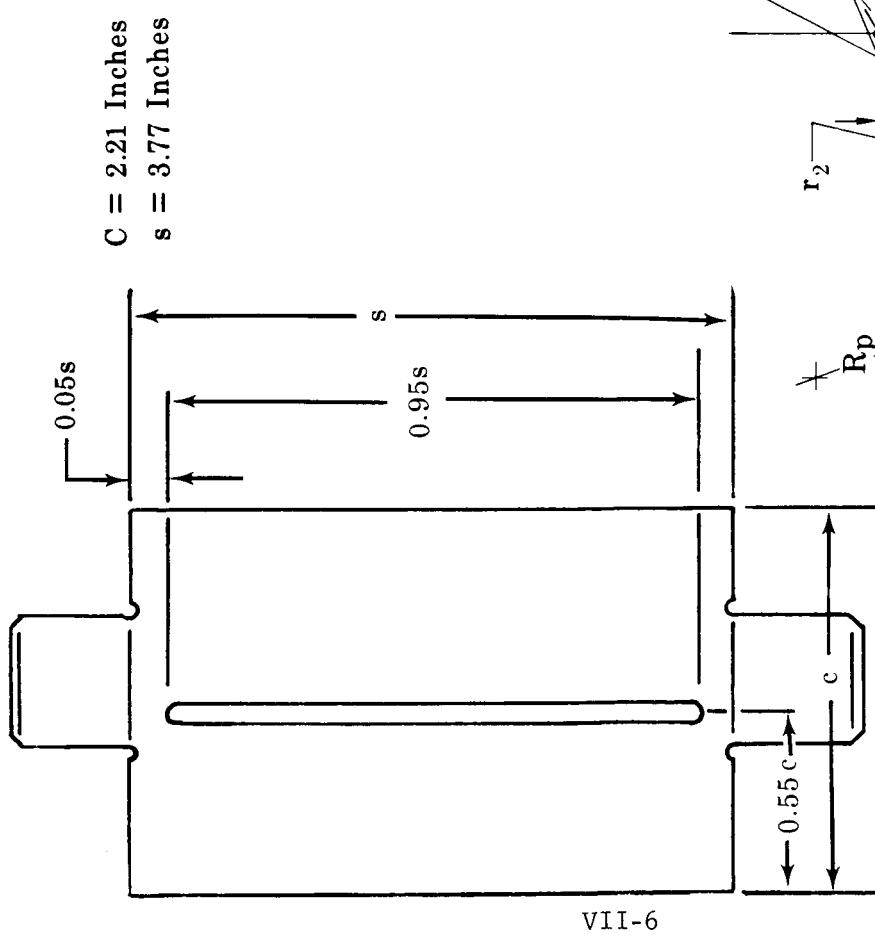


Figure III-4. Rotating Cascade Rig Bleed System

FD 14683B

DIMENSIONS	
y_2	0.050 in.
t	0.196 in.
R	0.152 in.
r_1	0.019 in.
y_1	0.094 in.
r_2	0.005 in.
R_p	0.332 in.
ψ	30°



VII-6

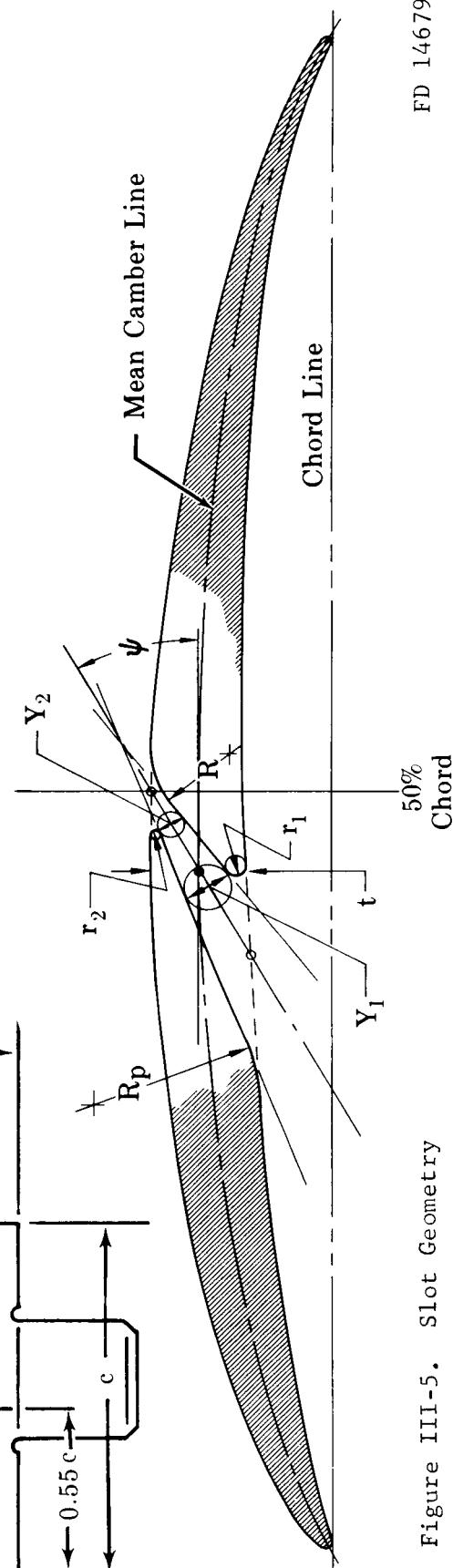
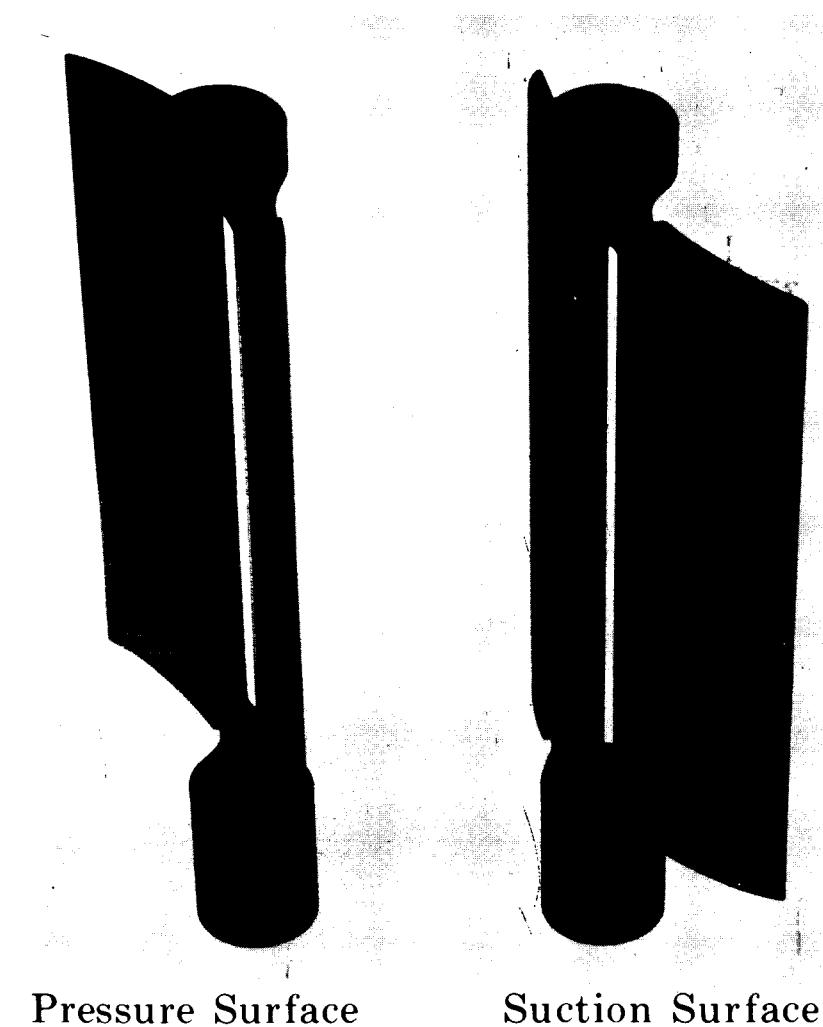


Figure III-5. Slot Geometry

FD 14679E

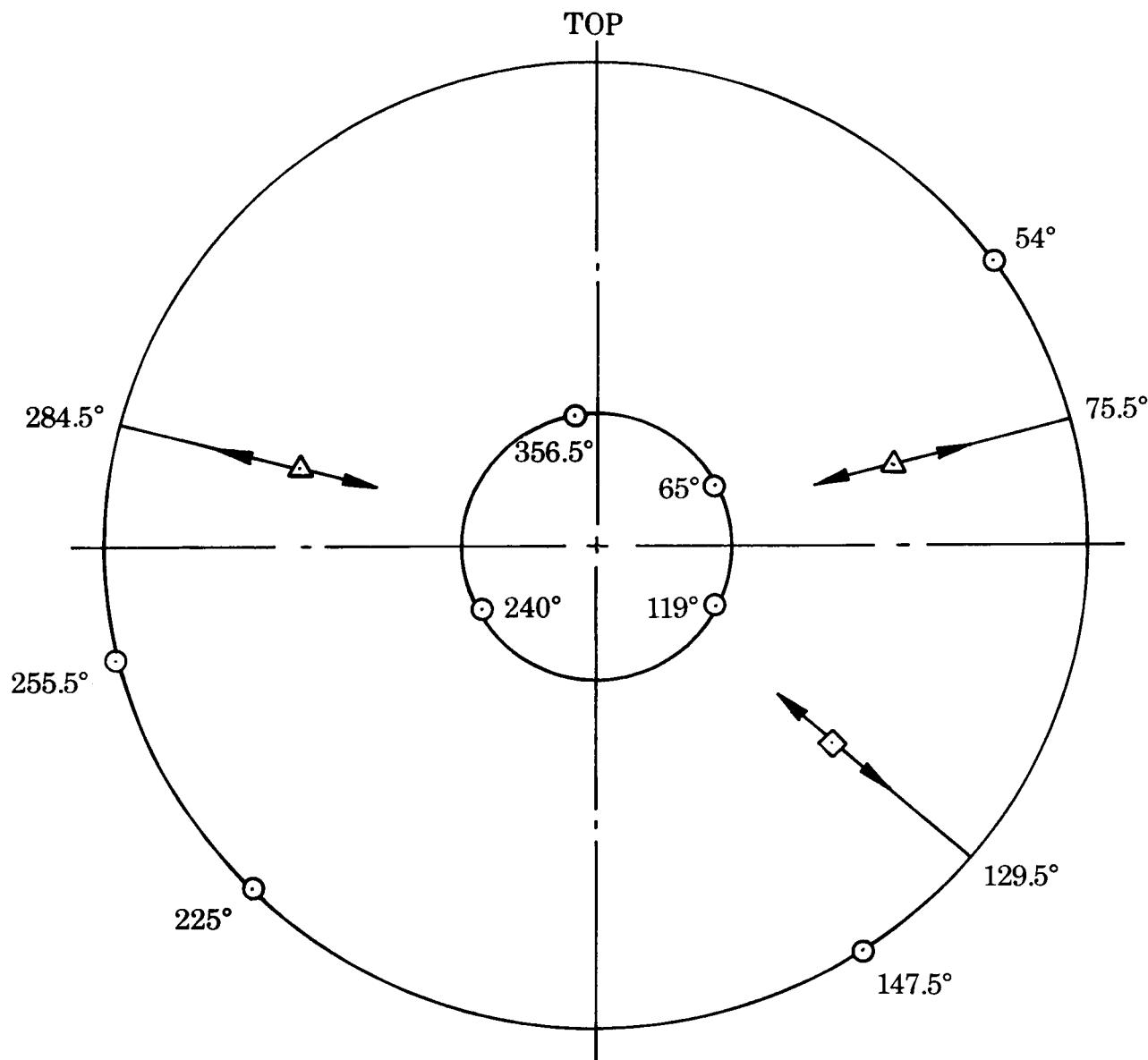


Pressure Surface

Suction Surface

Figure III-6. Typical Slotted Stator 3 Vane

FD 22751

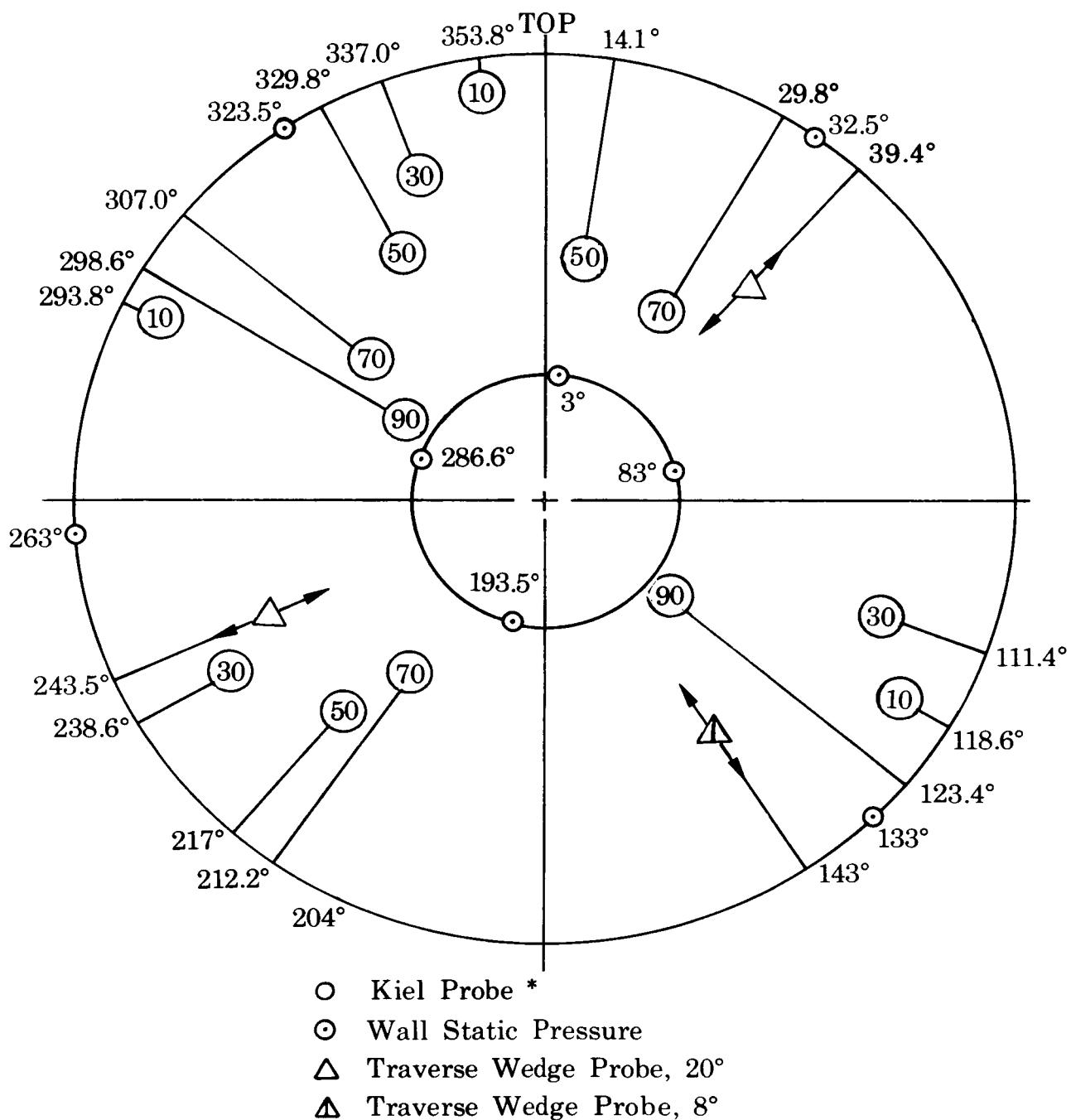


- Wall Static Pressure
- △ Traverse Wedge Probe, 20°
- ◇ Traverse Wake Probe

Probe angular position is measured clockwise from the top.

Figure III-7. Instrumentation, Station 1,
View Looking Downstream

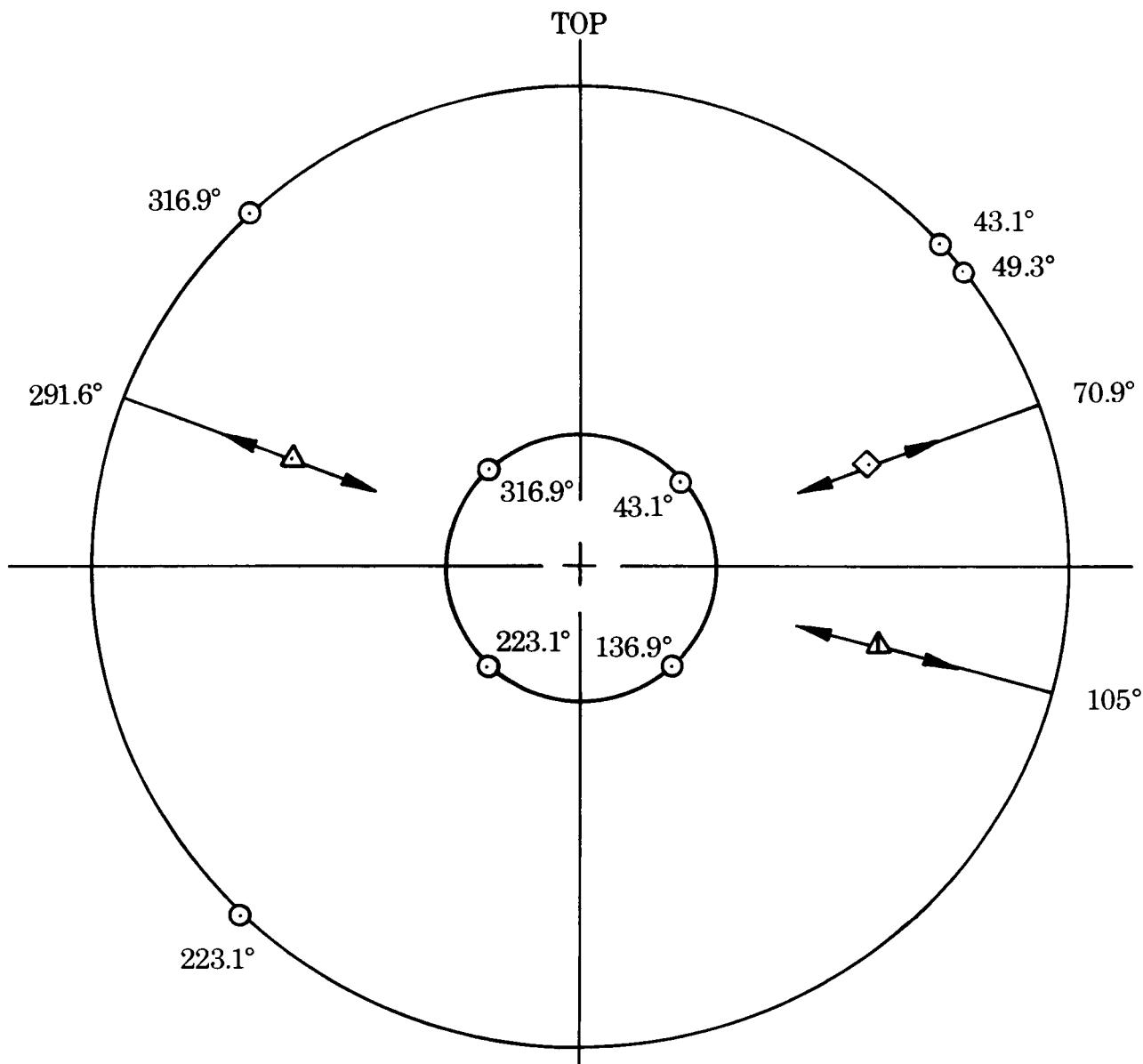
FD 18596C



*Radial location as a percent of span from tip is denoted by the number within the symbol

Figure III-8. Instrumentation, Station 2,
View Looking Downstream

FD 18595F



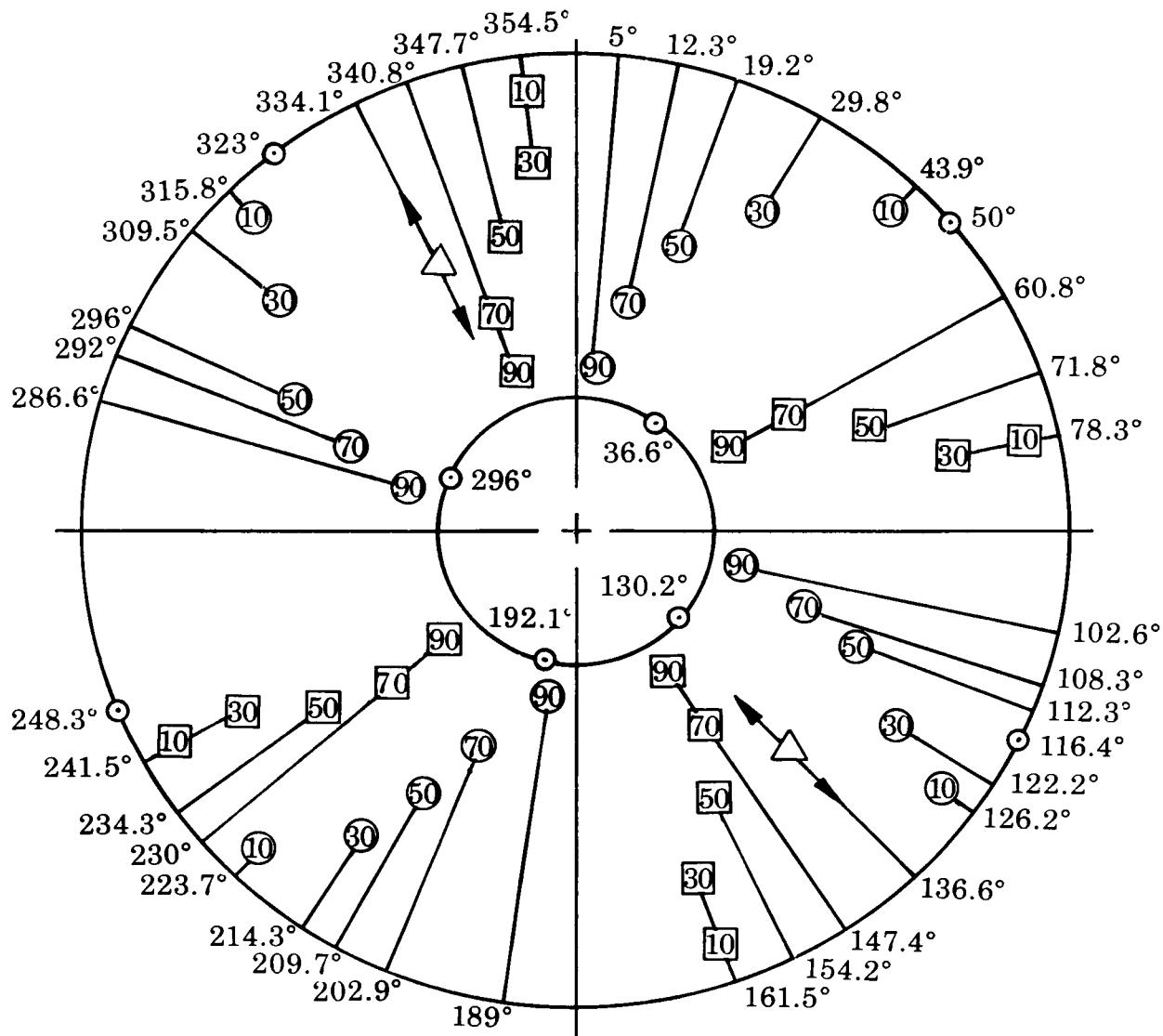
- Wall Static Pressure
- △ Traverse Wedge Probe, 20°
- ▲ Traverse Wedge Probe, 8°
- ◇ Traverse Wake Probe

Probe angular position is measured clockwise from the top.

Figure III-9. Instrumentation, Station 2A,
View Looking Downstream

FD 18594C

TOP



- Wall Static
- △ Traverse Wedge Probe, 20°
- △ Traverse Wedge Probe, 8°
- Kiel Probe *
- Temperature *

*Radial location as a percent of span from tip is denoted by the number within the symbol

Figure III-10. Instrumentation, Station 3,
View Looking Downstream

FD 18597C

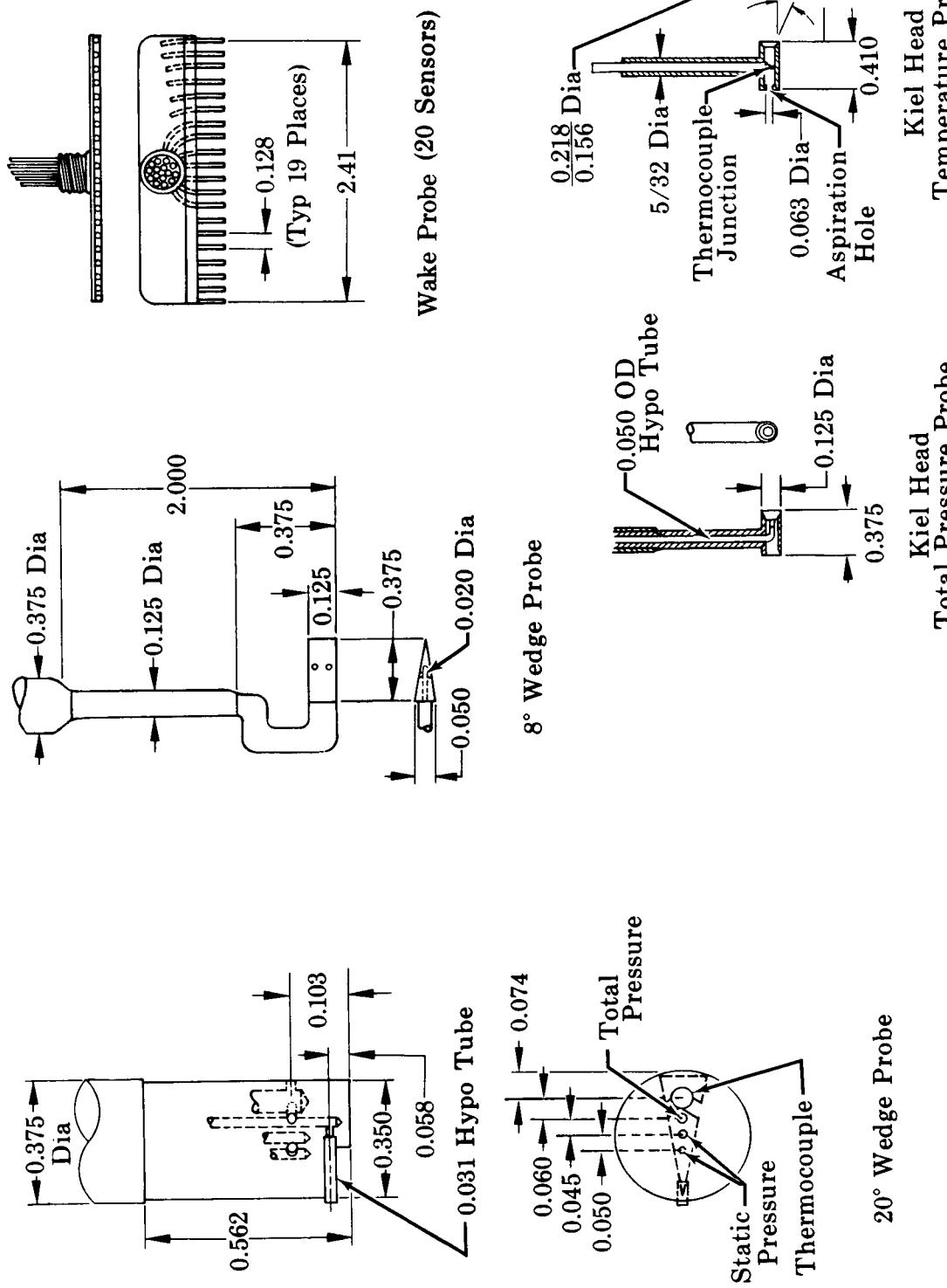


Figure III-11. Probe Configurations

Note: All Dimensions Are in Inches.
FD 18483B

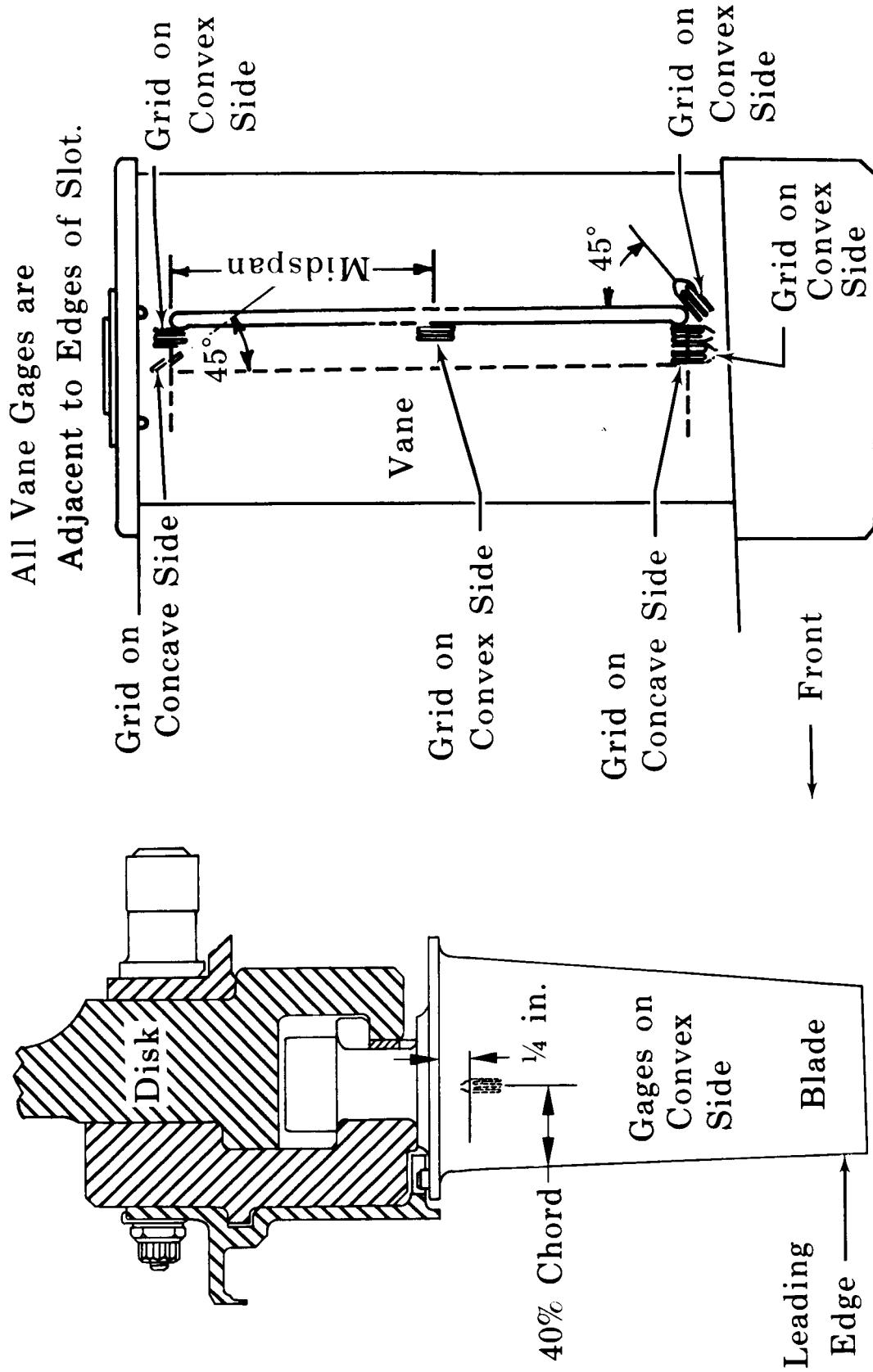


Figure III-12. Strain Gage Locations

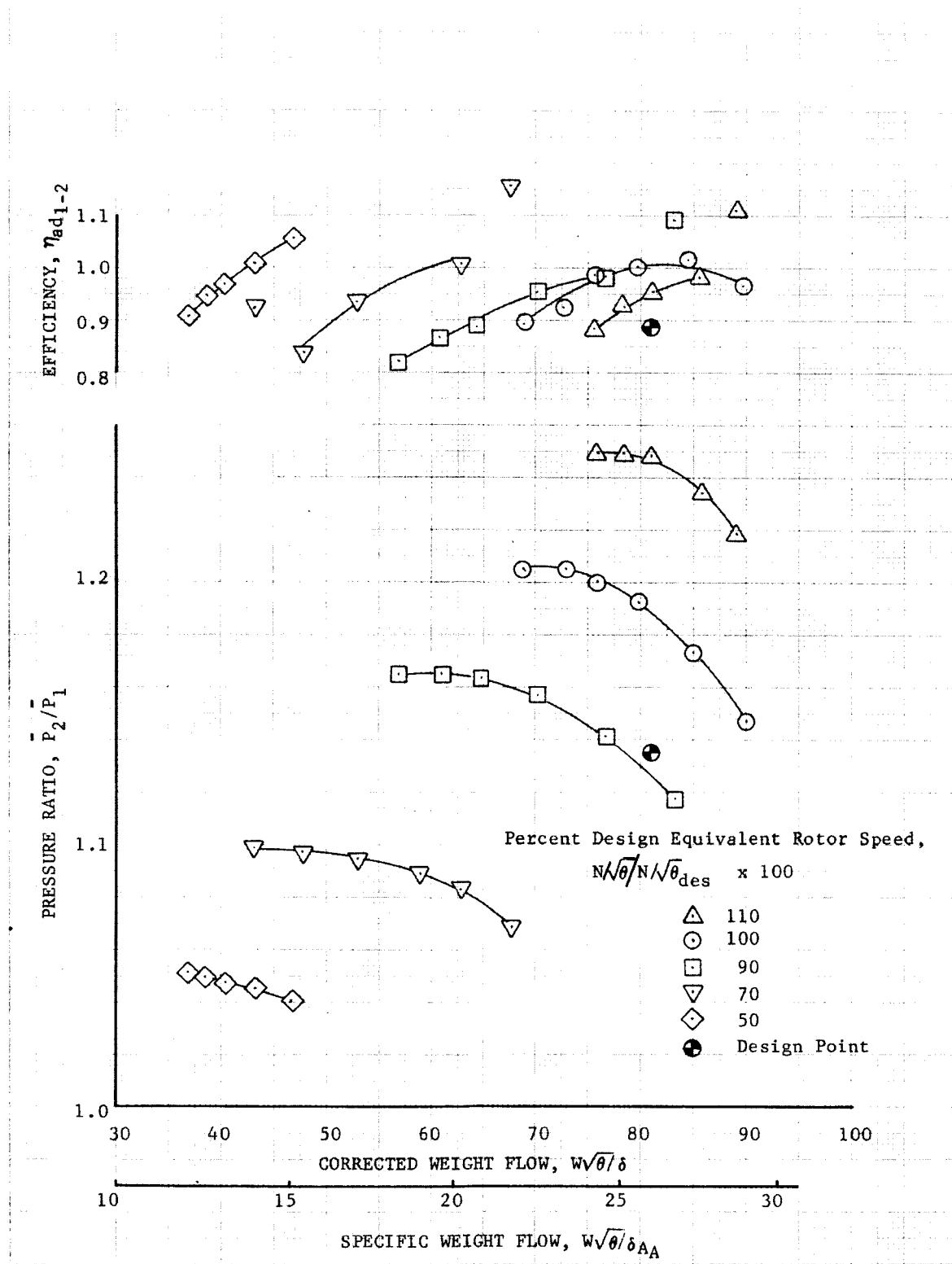


Figure V-1. Overall Performance: Flow Generation Rotor Only

DF 58413

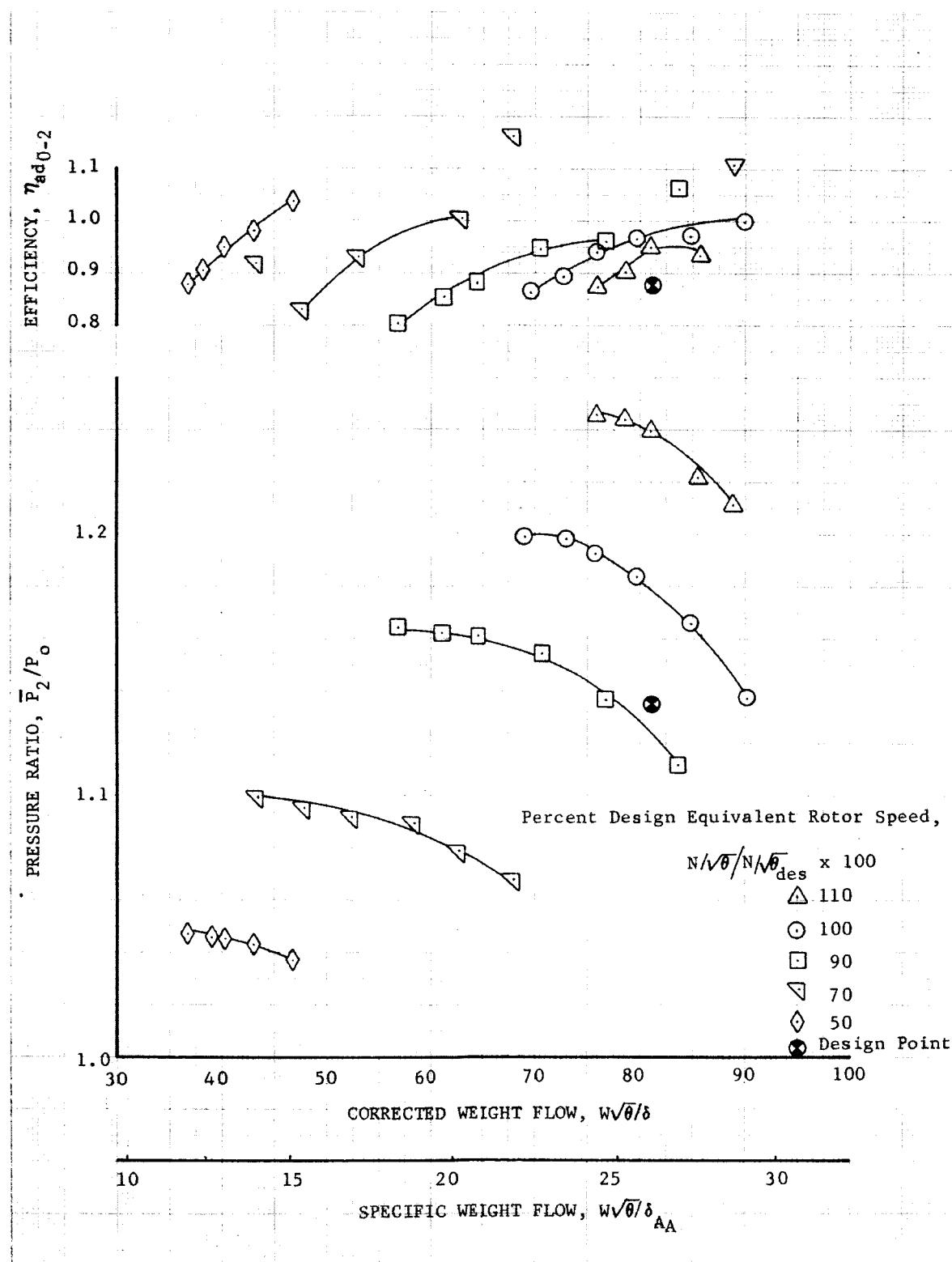


Figure V-2. Overall Performance: Guide Vane, Flow Generation Rotor

DF 58414

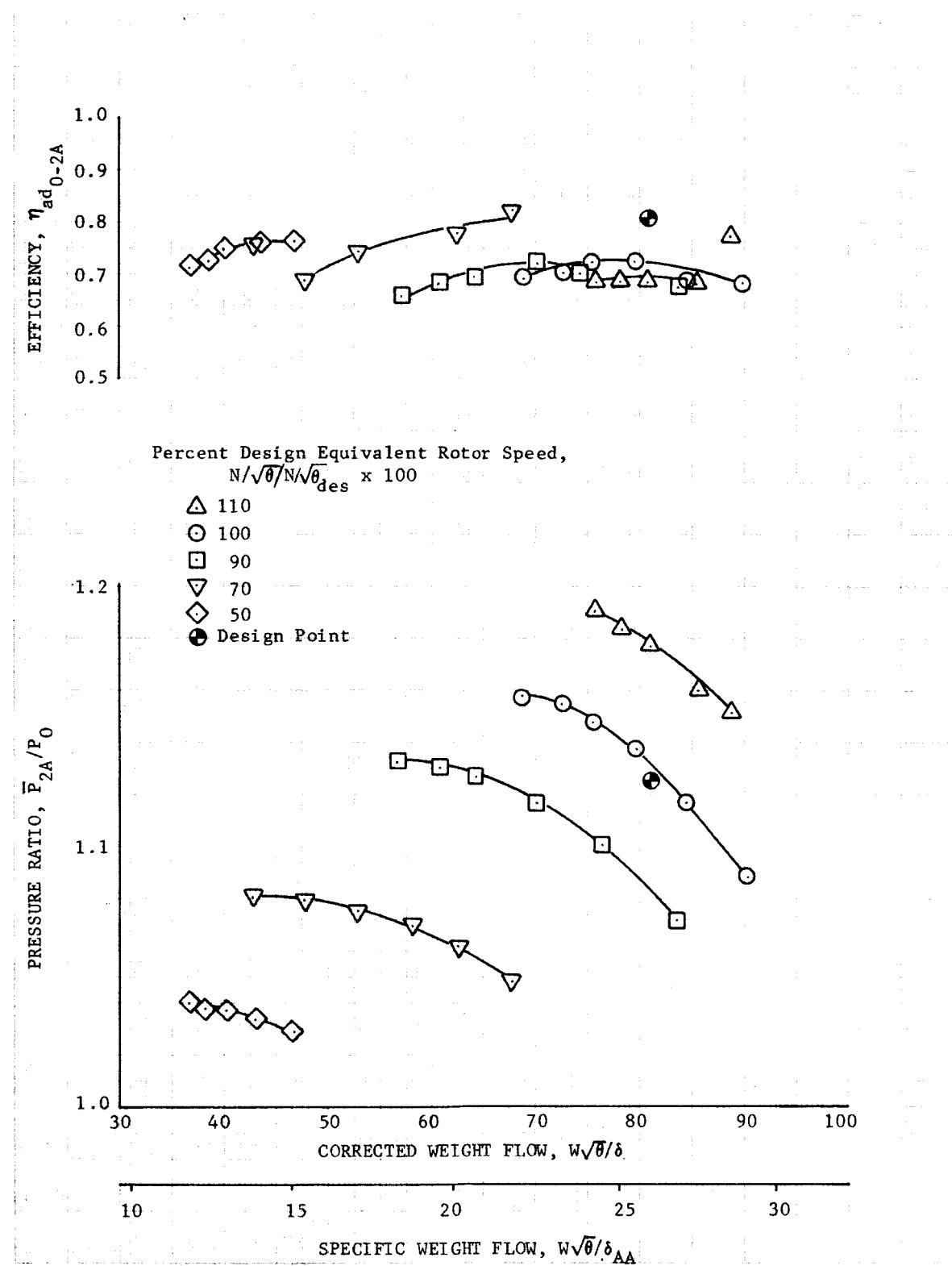


Figure V-3. Overall Performance: Guide Vane, Flow Generation Rotor, Slotted Stator 3

DF 58415

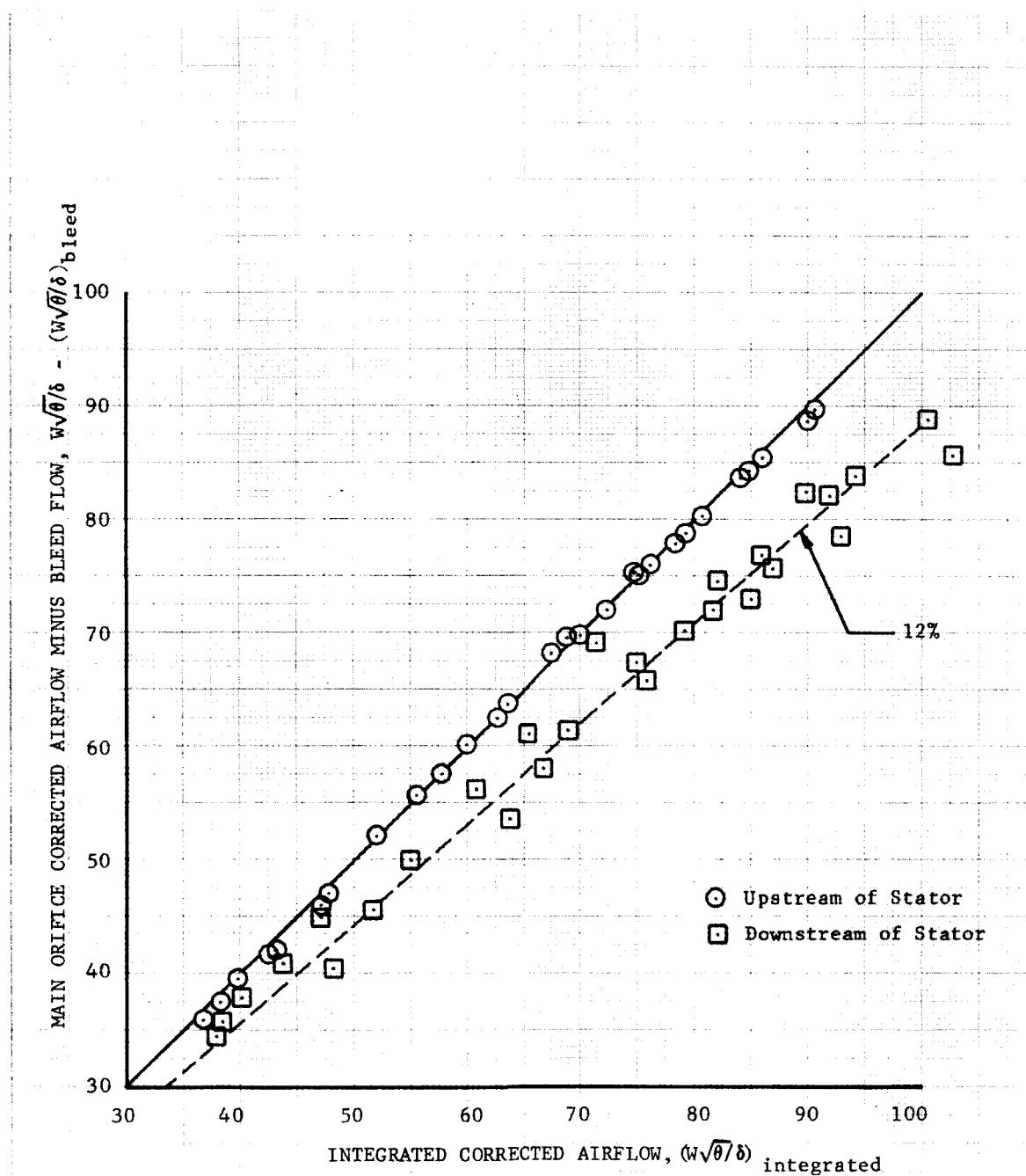


Figure V-4. Airflow Continuity Comparison

DF 58416

DF 58417

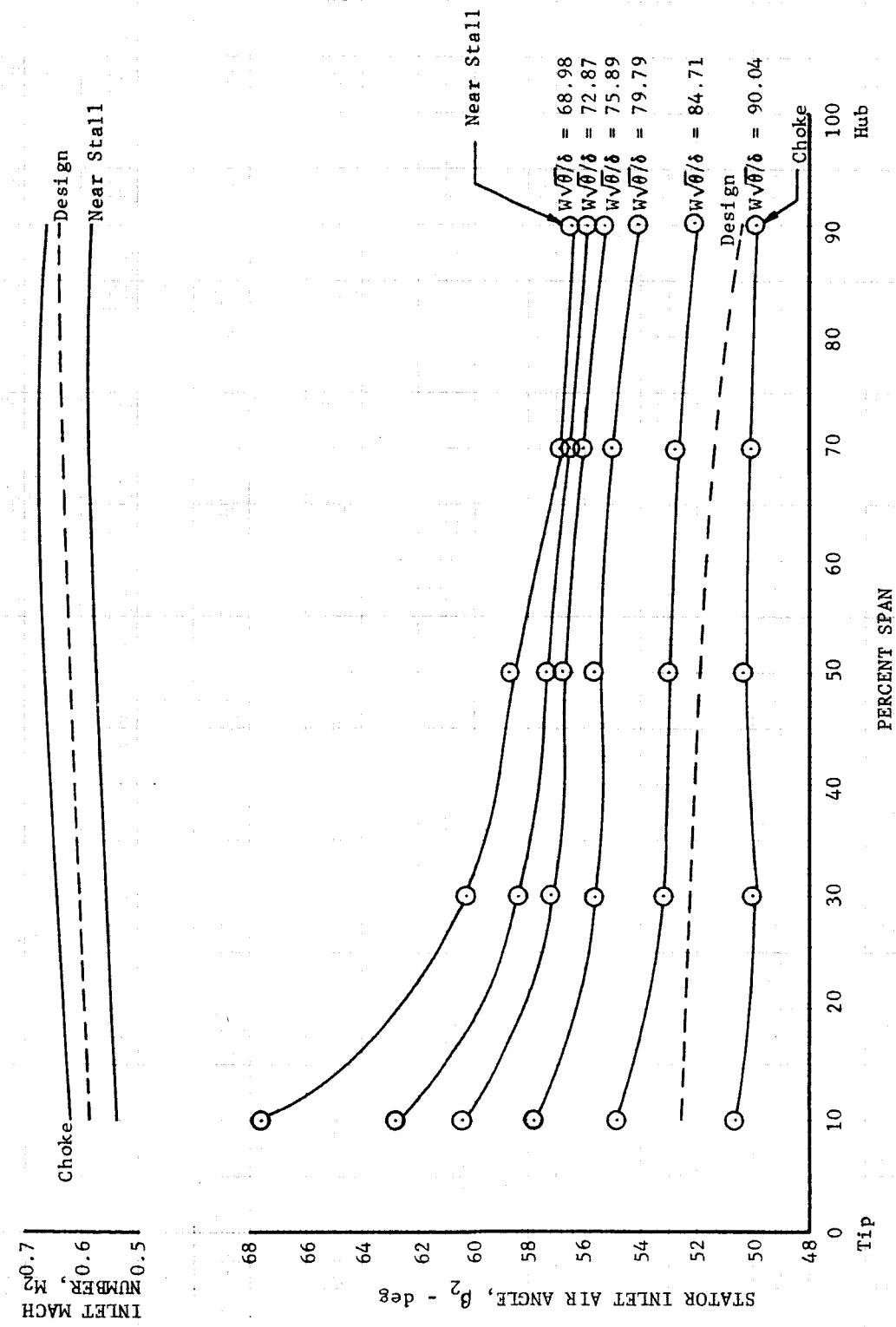


Figure V-5. Stator Inlet Air Angle and Mach Number Distribution: 100% Design Equivalent Rotor Speed

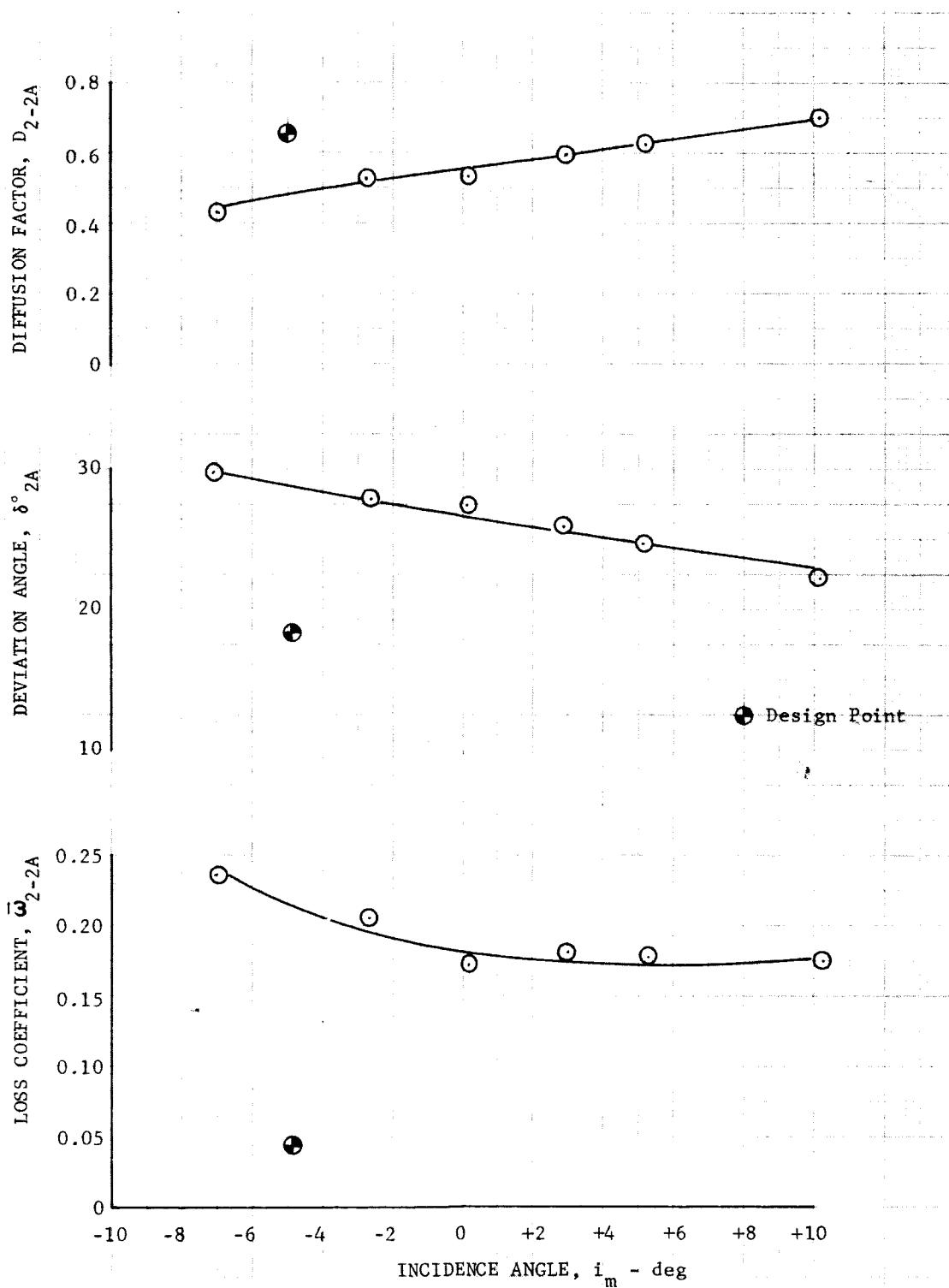


Figure V-6. Stator Blade Element Performance: 100% Design DF 58418
Equivalent Rotor Speed, 10% Span From Tip

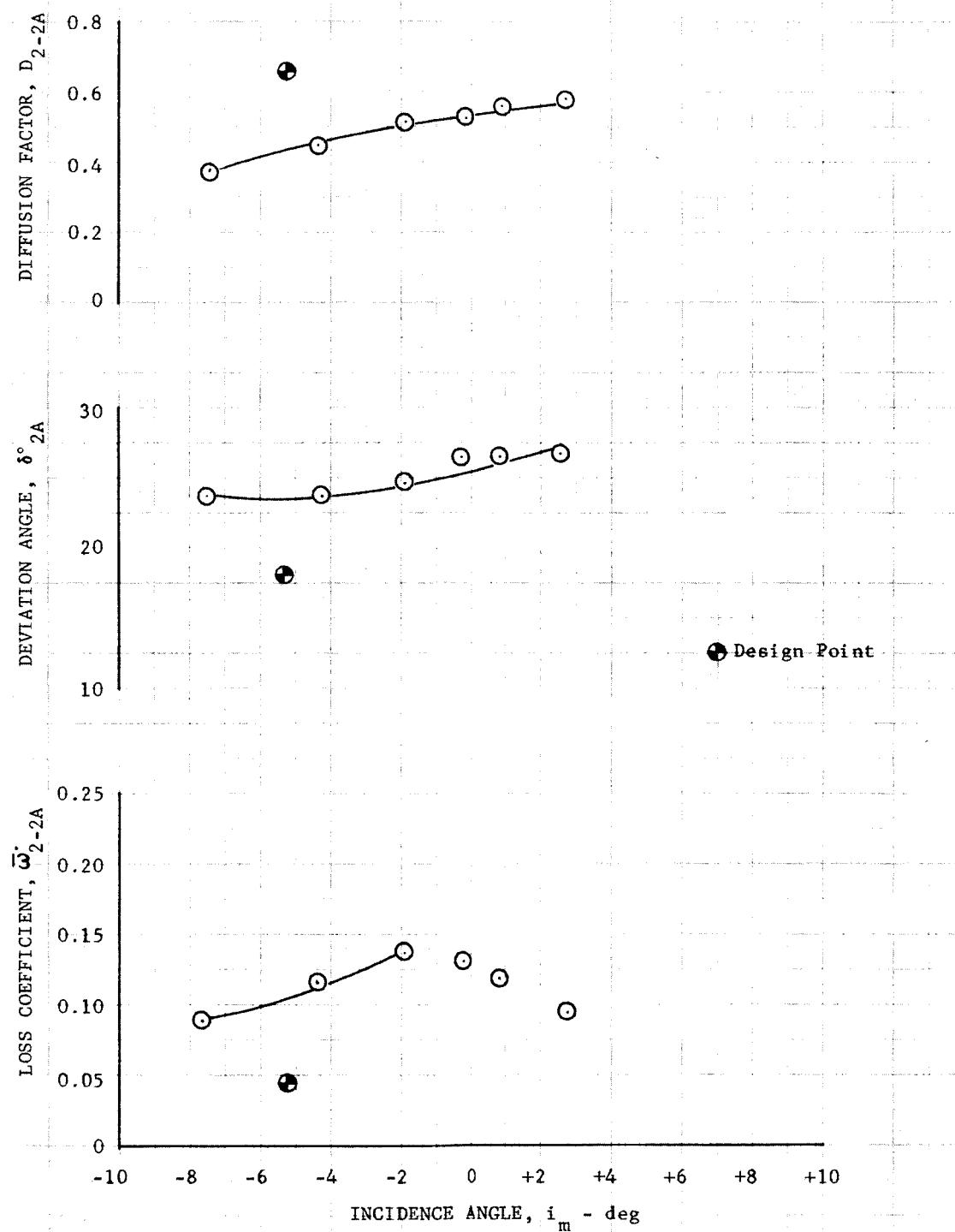


Figure V-7. Stator Blade Element Performance: 100% Design
Equivalent Rotor Speed, 30% Span From Tip

DF 58419

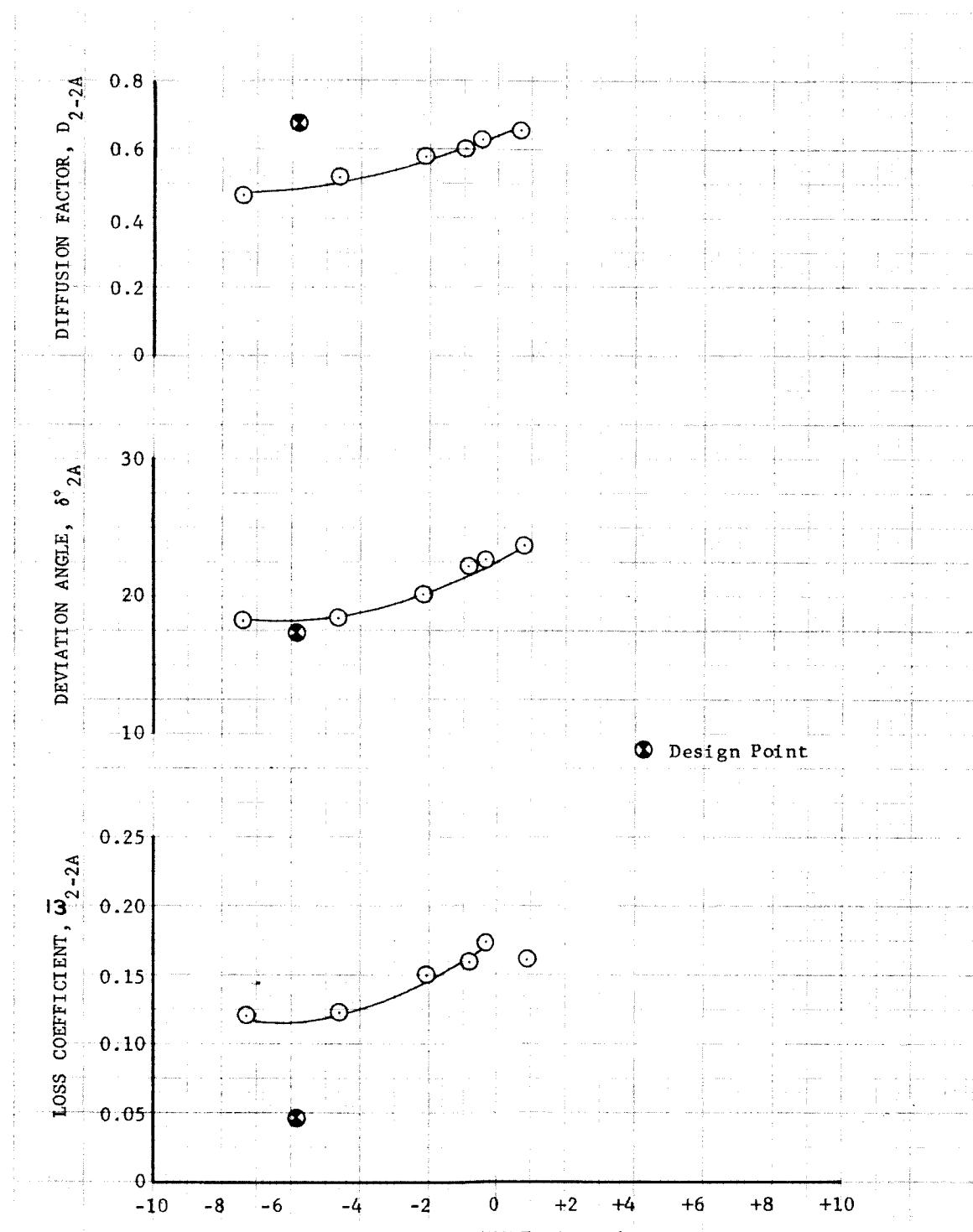


Figure V-8. Stator Blade Element Performance: 100% Design
Equivalent Rotor Speed, 50% Span From Tip

DF 58420

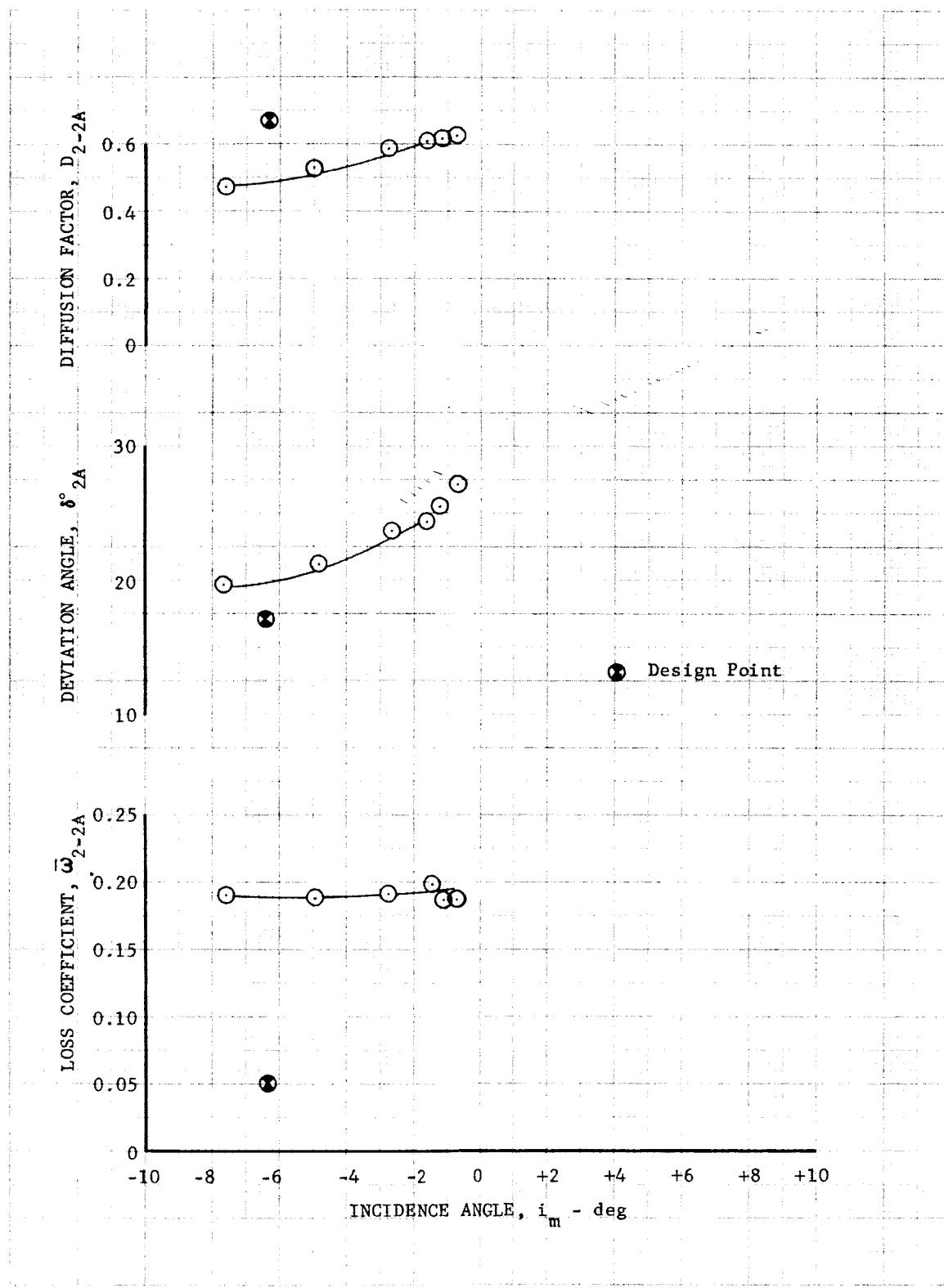


Figure V-9. Stator Blade Element Performance: 100% Design
Equivalent Rotor Speed, 70% Span From Tip

DF 58421

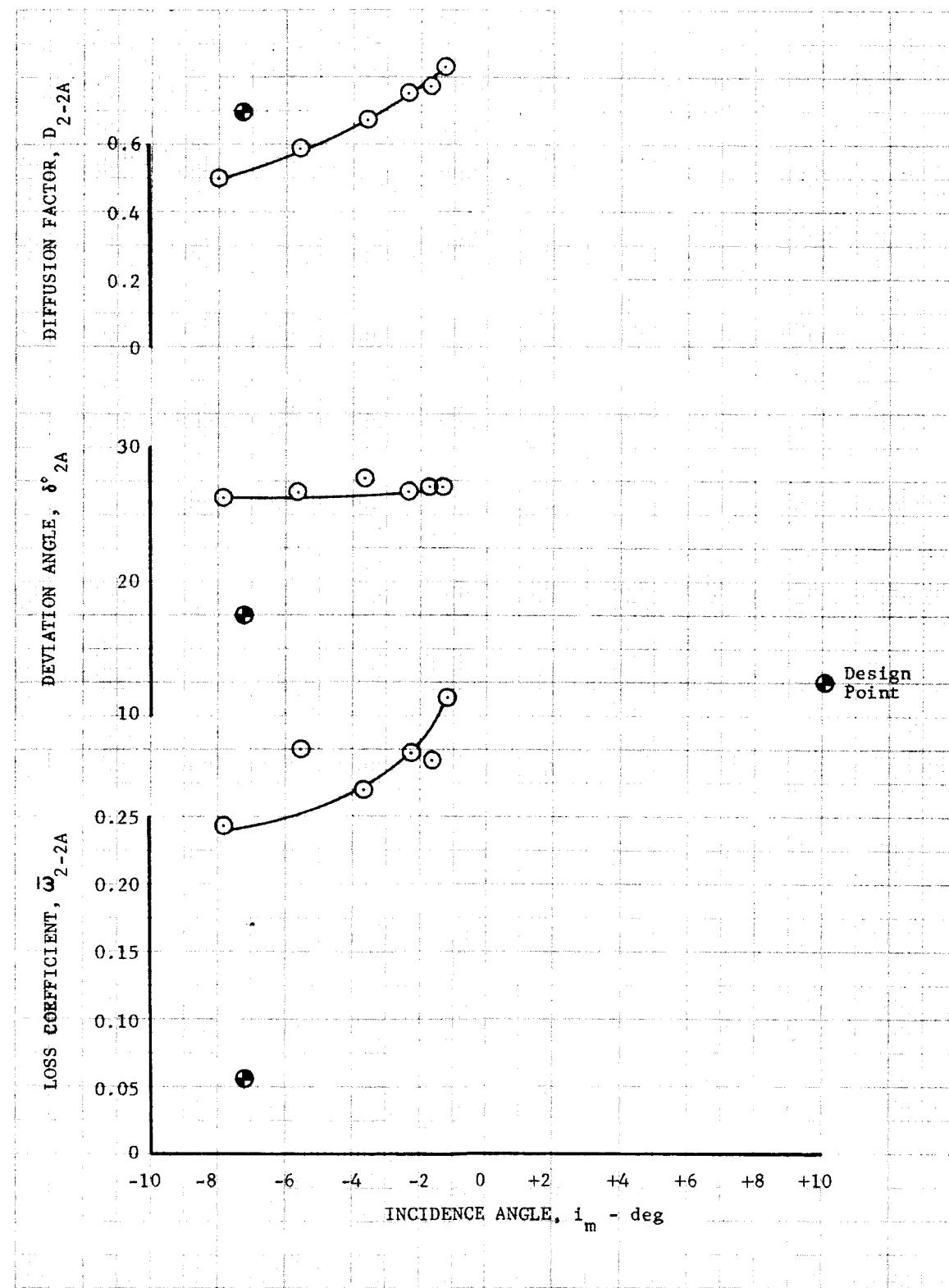


Figure V-10. Stator Blade Element Performance : 100% Design
Equivalent Rotor Speed, 90% Span From Tip

DF 58422

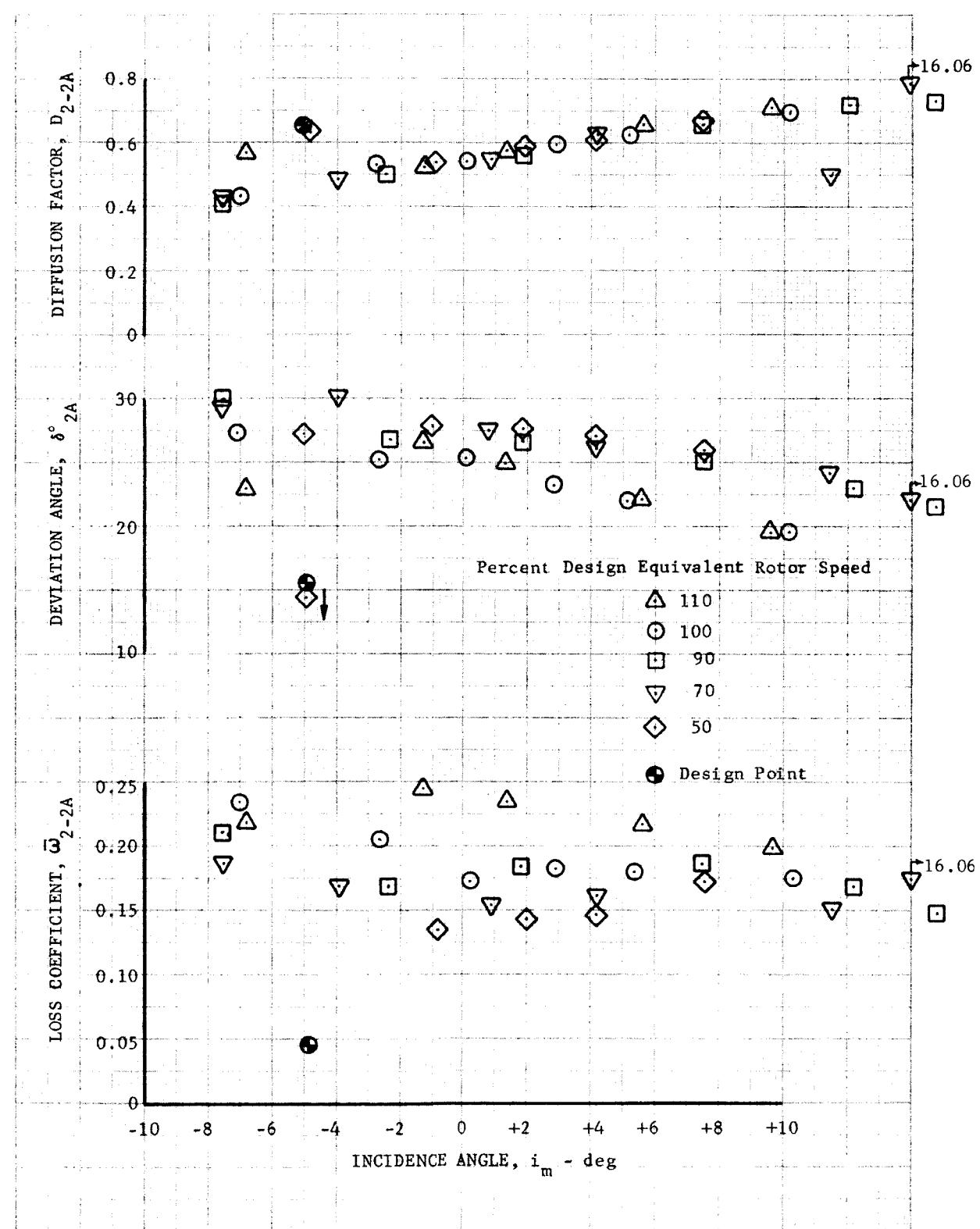


Figure V-11. Variation of Stator Blade Element Parameters
With Incidence: Slotted Stator 3, 10% Span
From Tip

DF 58423

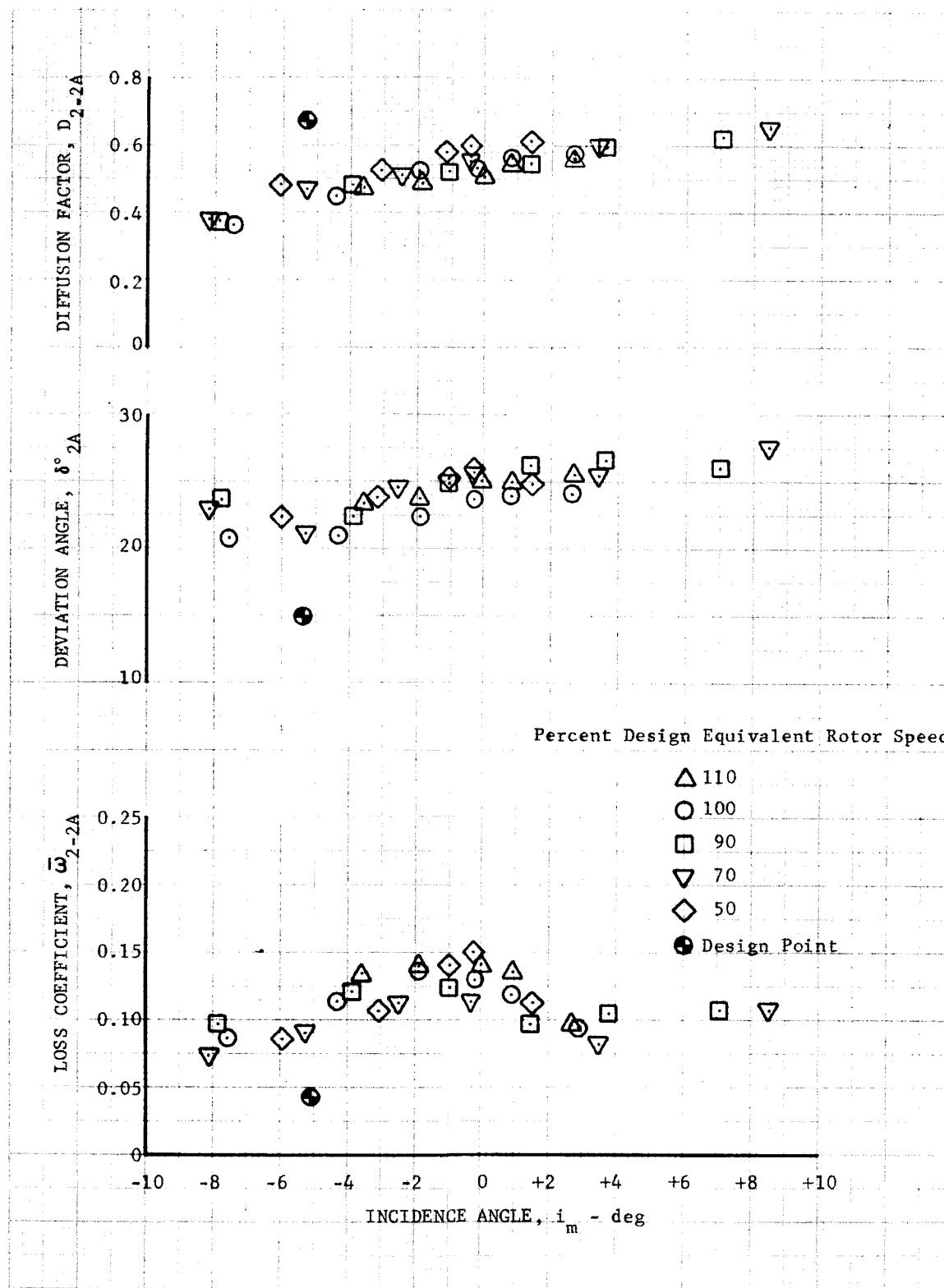


Figure V-12. Variation of Stator Blade Element Parameters With Incidence: Slotted Stator 3, 30% Span From Tip

DF 58424

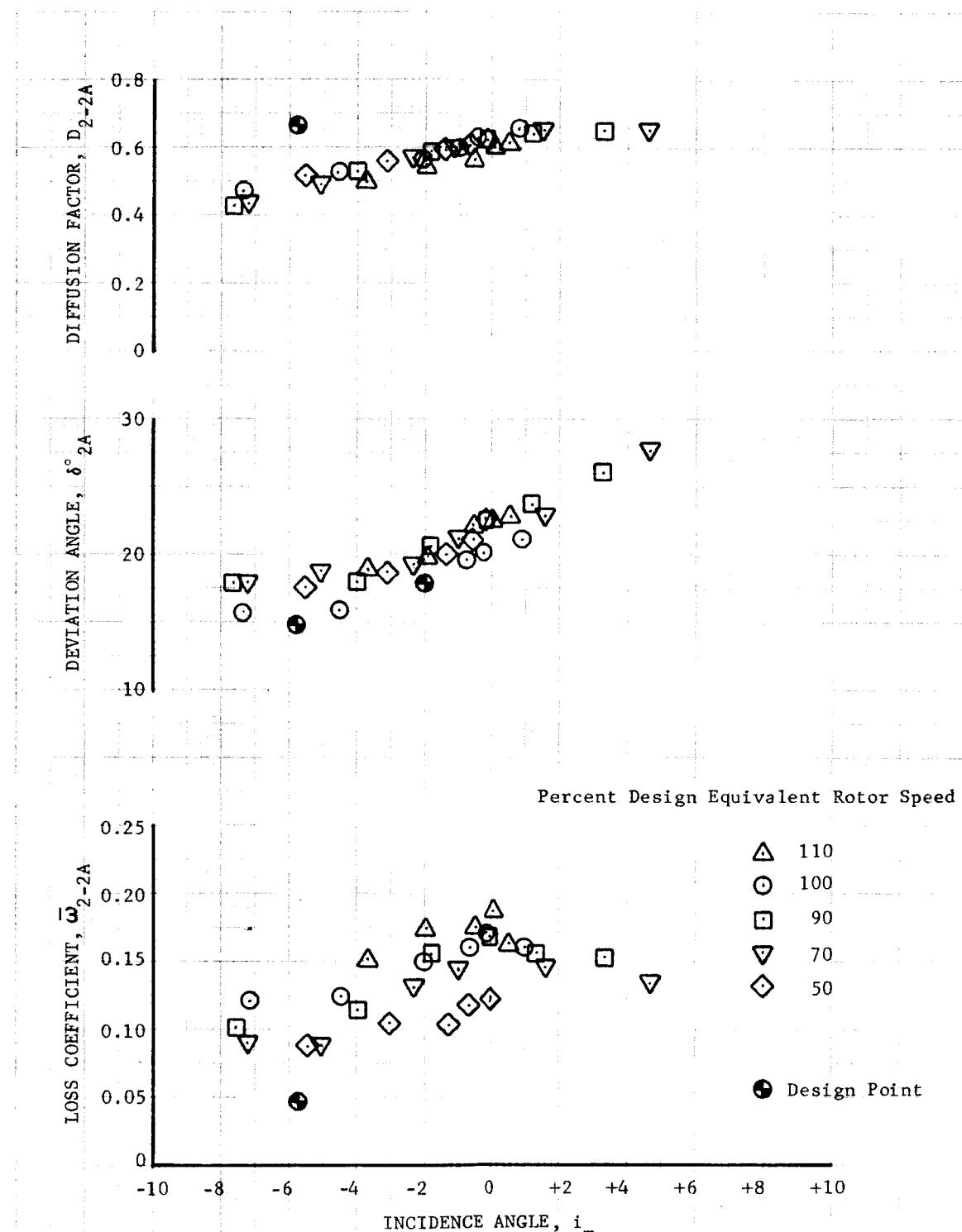


Figure V-13. Variation of Stator Blade Element Parameters
With Incidence: Slotted Stator 3, 50% Span
From Tip

DF 58425

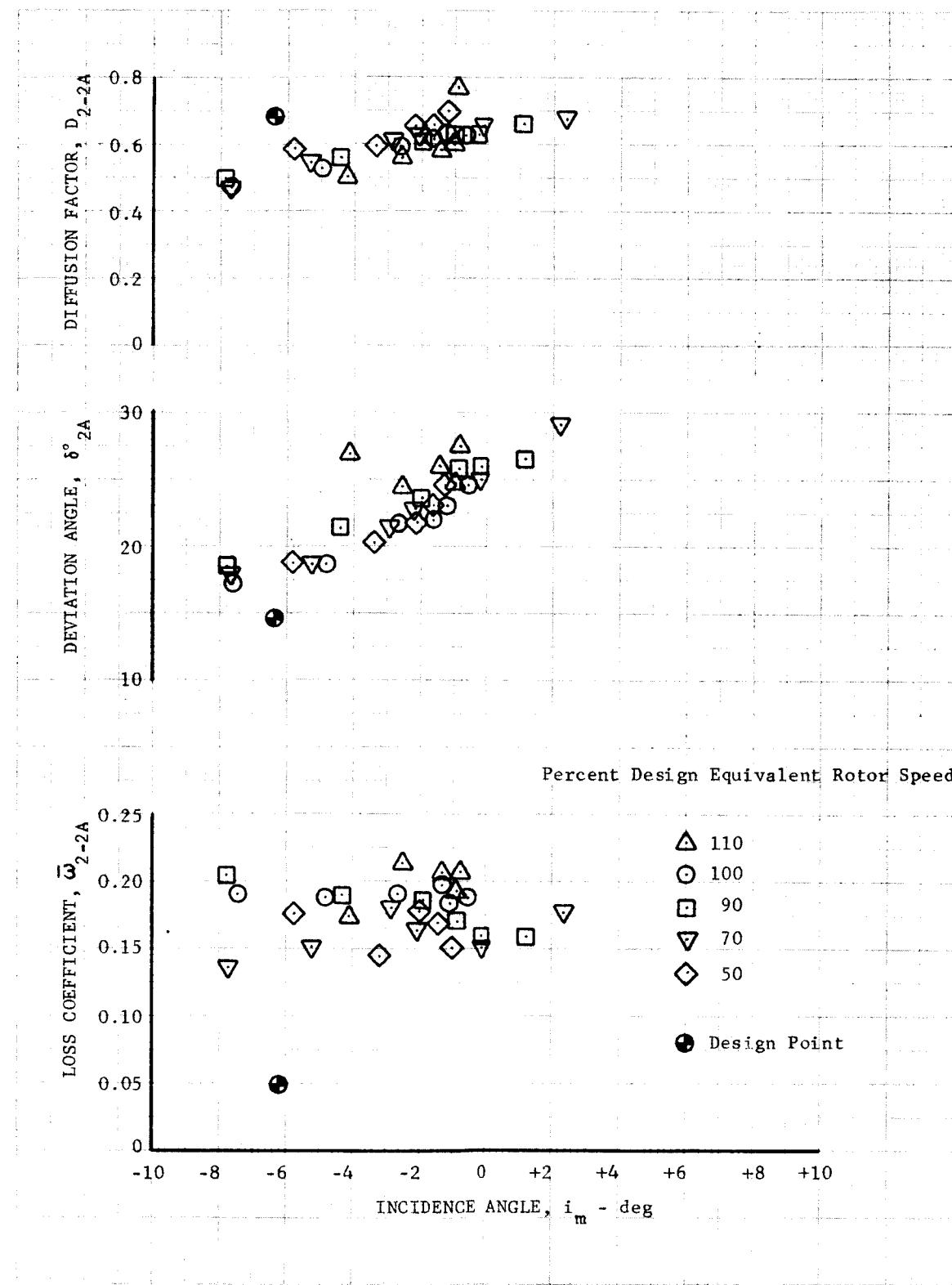


Figure V-14. Variation of Stator Blade Element Parameters
With Incidence: Slotted Stator 3, 70% Span
From Tip

DF 58426

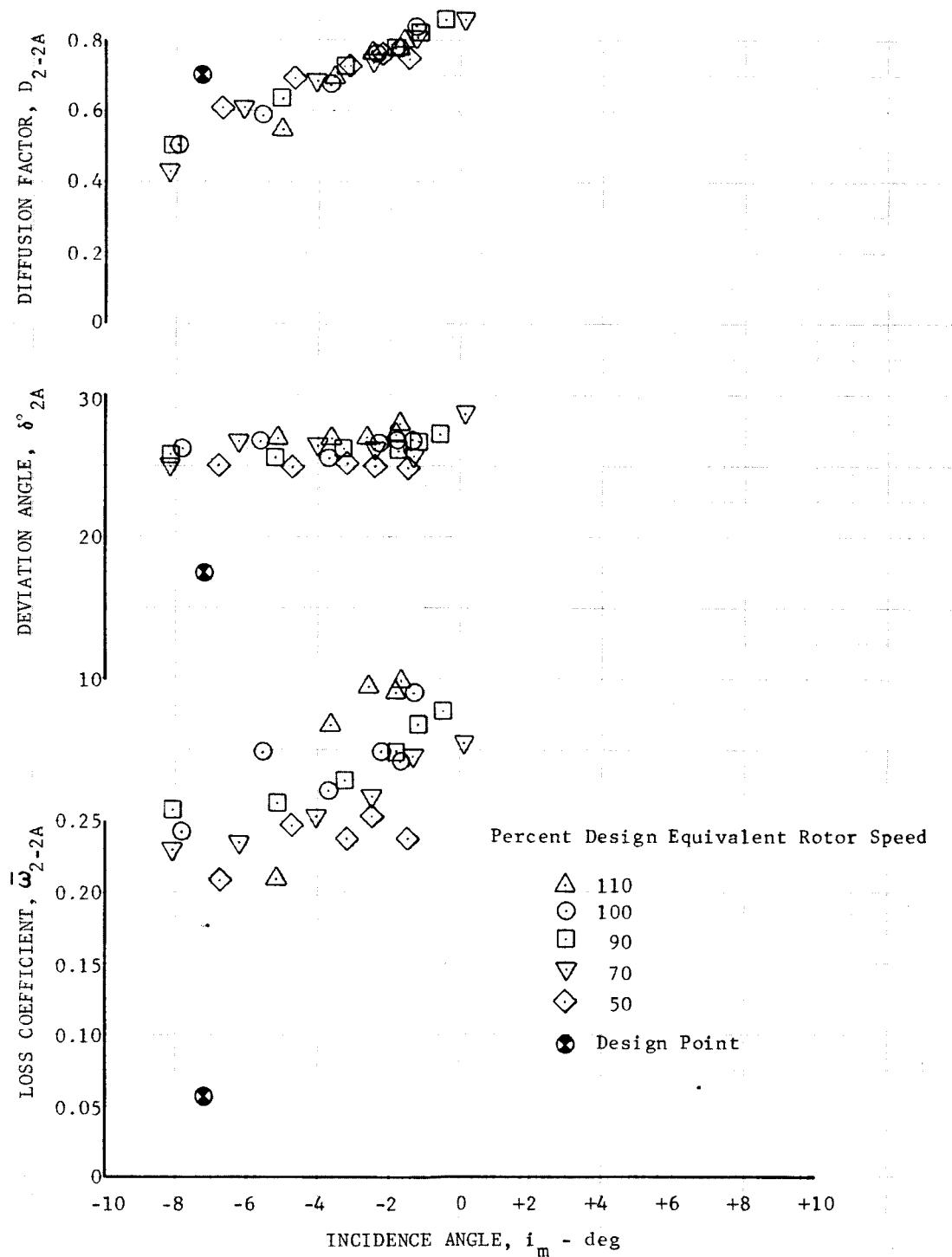


Figure V-15. Variation of Stator Blade Element Parameters
With Incidence: Slotted Stator 3, 90% Span
From Tip

DF 58427

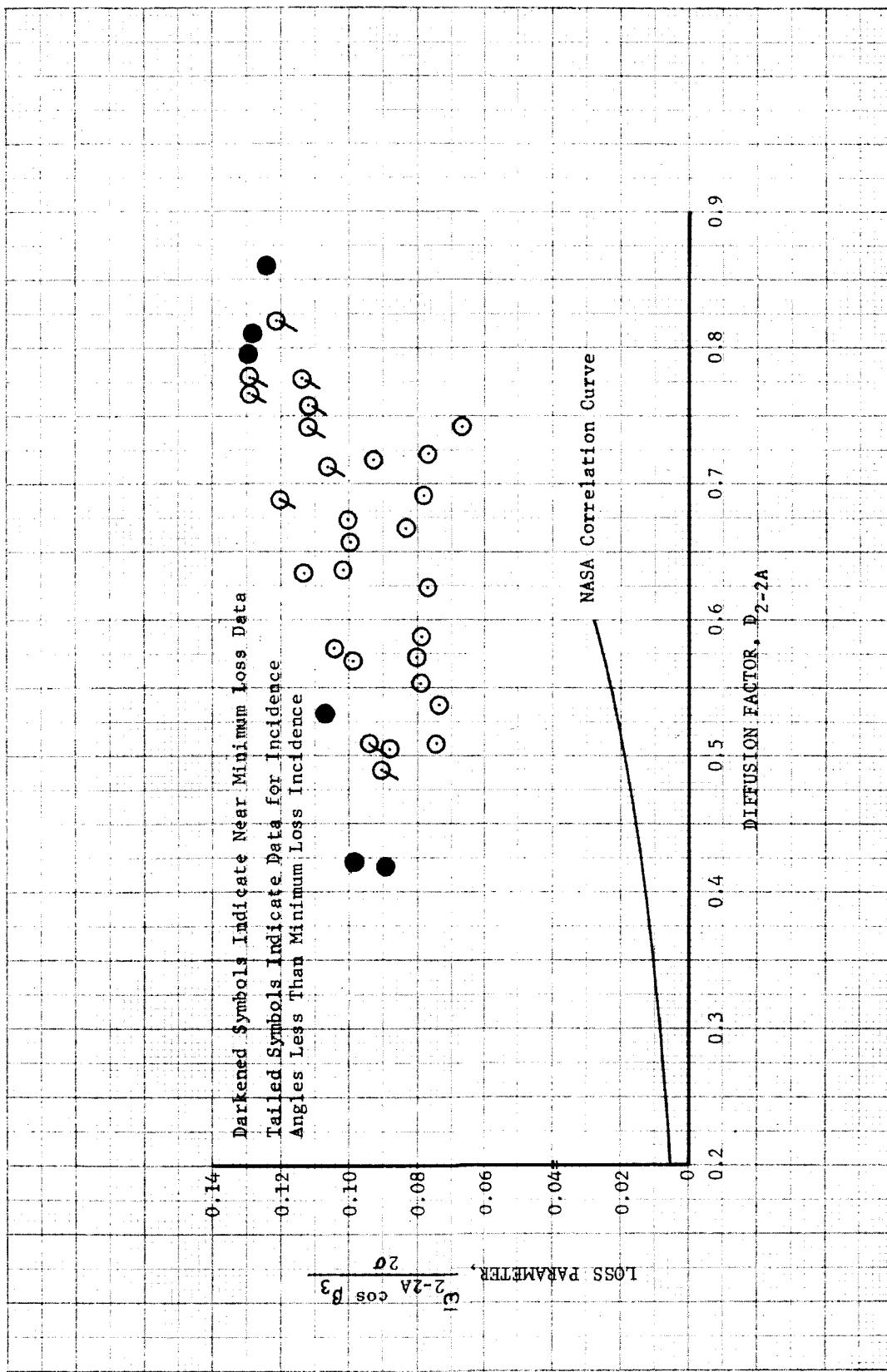


Figure V-16a. Loss Parameter versus Diffusion Factor: 90 and 10% Span (From Tip); 90, 100, and 110% Design Equivalent Rotor Speed

DF 58428

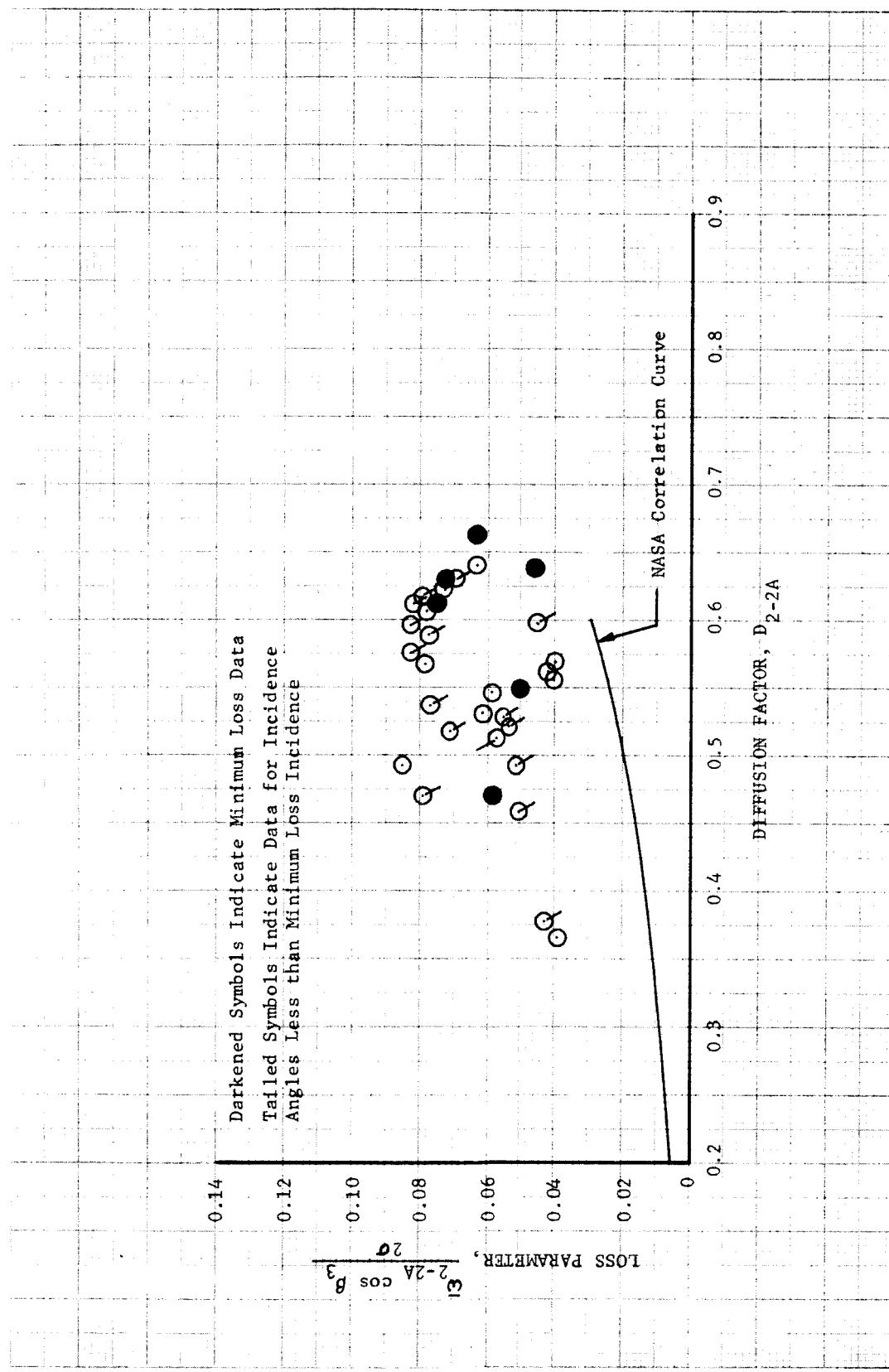


Figure V-16b. Loss Parameter versus Diffusion Factor: 70 and 30% Span (From Tip); 90, 100, and 110% Design Equivalent Rotor Speed
DF 58429

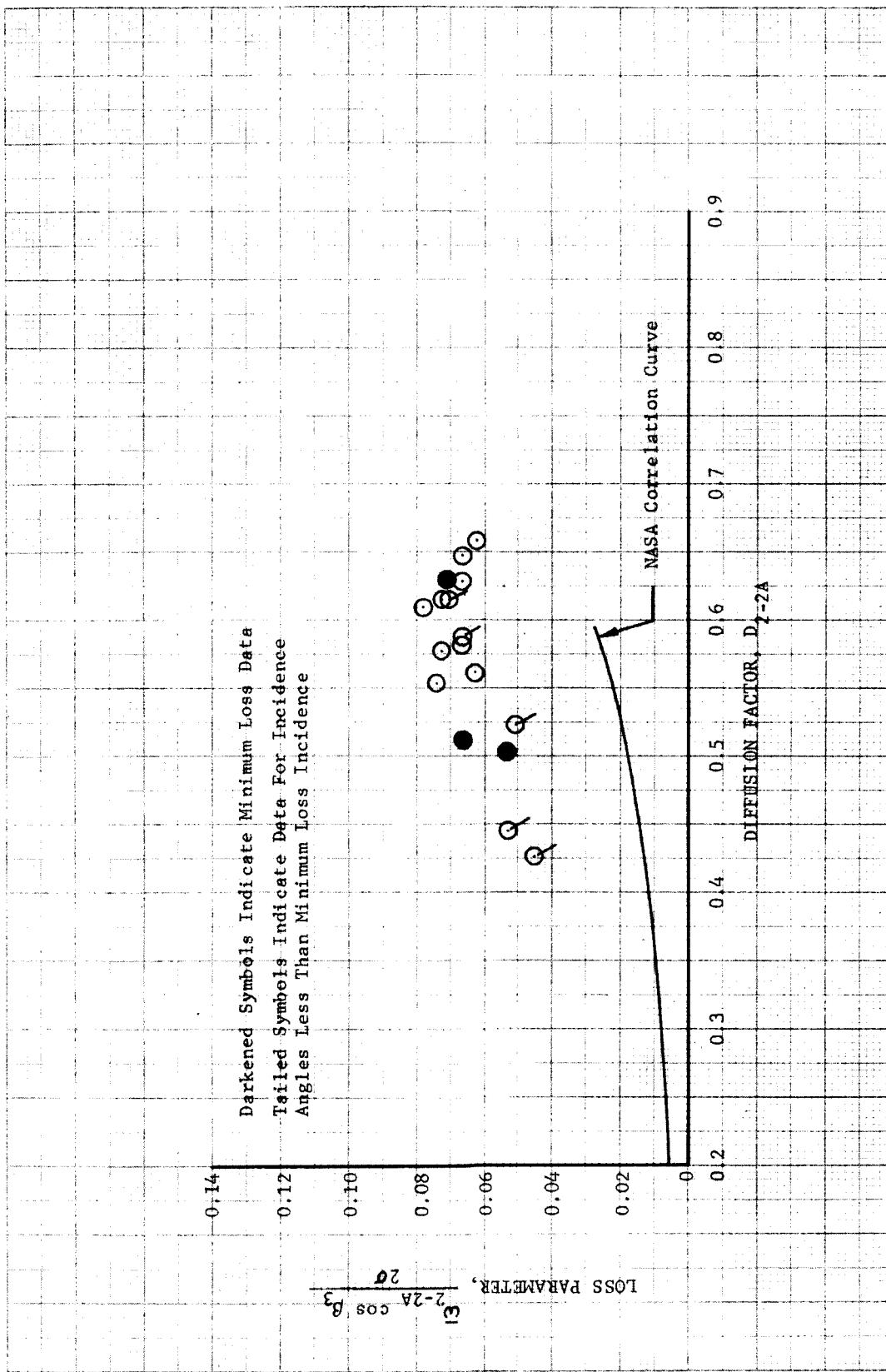


Figure V-16c. Loss Parameter versus Diffusion Factor: 50% Span (From Tip); 90, 100, and 110% Design Equivalent Rotor Speed

DF 58430

APPENDIX A
DEFINITION OF SYMBOLS

A. GENERAL NOMENCLATURE

A_A	Flow path annular area, in. ²
c	Chord length, in.
D	Diffusion factor
i_m	Incidence angle based on an equivalent circular arc, deg
M	Absolute Mach number
o	Minimum blade passage gap, in.
o^*	Critical blade passage gap, in.
P	Total pressure, psia
p	Static pressure, psia
q	Pressure equivalent of the velocity head, psia
R	Reynolds number based on chord length
S	Blade spacing, in.
s	Blade span, in.
T	Total temperature, °R
t	Blade maximum thickness, in.
U	Rotor speed, ft/sec
V	Absolute velocity, ft/sec
W	Actual flow rate, lb _m /sec
β	Absolute air angle, deg
γ	Ratio of specific heats
γ^o	Blade-chord angle, deg
δ	Ratio of total pressure to NASA standard sea level pressure of 2116 psf
δ^o	Deviation angle, deg
η_{ad}	Adiabatic efficiency
θ	Ratio of total temperature to NASA standard sea level temperature of 518.7°R
κ	Blade metal angle, deg
ρ	Density, lb _m /ft ³
σ	Solidity, c/S

ϕ Blade camber angle, $K_1 - K_2$, deg

$\bar{\omega}$ Total pressure loss coefficient

Subscripts:

0	Guide vane inlet
1	Rotor inlet
2	Rotor exit
2A	Stator exit
3	Downstream of stator exit
z	Axial component
θ	Tangential component

Superscripts:

'	Related to rotor blade
-	Mass average value

B. SLOT NOMENCLATURE

A_2	Slot throat area, in. ²
R	Coanda radius, in.
R_p	Pressure surface edge radius, in.
r_1	Slot leading edge radius, in.
r_2	Slot trailing edge radius, in.
t	Blade thickness at intersection of slot centerline and mean camber line, in.
Y_1	Slot capture dimension, in.
Y_2	Slot throat dimension, in.
ψ	Angle formed by slot centerline and mean camber line, deg

C. BLADE ELEMENT TABULATION NOMENCLATURE FOR TABLE B-2

PCT SPAN	Percent span
DIA	Diameter, inches
BETA	Absolute air angle, degrees
BETA(PR)	Relative air angle, degrees
V	Absolute velocity, ft/sec

VZ	Axial component of velocity, ft/sec
V-THETA	Tangential component of absolute velocity, ft/sec
V(PR)	Relative velocity, ft/sec
V-THETA PR	Tangential component of relative velocity, ft/sec
U	Wheel speed, ft/sec
M	Absolute Mach number
M(PR)	Relative Mach number
TURN	Air turning, degrees
TURN(PR)	Relative air turning, degrees
UUBAR	Loss coefficient
DFAC	Diffusion factor
EFFP	Polytropic efficiency
EFF	Adiabatic efficiency
INCID	Incidence, degrees
DEV	Deviation, degrees
LOSS PARA	Loss parameter

APPENDIX B
TABULATED PERFORMANCE

The overall performance and percent rotor and stator bleed flow rates for each test point are presented in table B-1.

Table B-2 presents blade element data for each test point. Definitions of the blade element parameters as tabulated in the computer printouts are presented in Appendix A.

Table B-1. Tabulation of Overall Performance and Percent Bleed

Corrected Main Orifice Weight Flow $W\sqrt{\theta}/\delta$, lb _m /sec	Overall Performance						Percent Bleed Rotor Stator	
	Stage		Flow Generation Rotor					
	\bar{P}_{2A}/P_0	η_{ad0-2A} , %	\bar{P}_2/\bar{P}_1	η_{ad1-2} , %				
50% Design Equivalent Rotor Speed								
36.68	1.040	71.53	1.051	90.90		1.960	4.53	
38.20	1.038	72.66	1.049	94.06		1.810	4.35	
40.22	1.037	75.34	1.048	96.26		1.670	3.92	
43.15	1.035	77.07	1.046	100.46		1.440	3.28	
46.75	1.029	76.20	1.041	105.89		1.270	2.65	
70% Design Equivalent Rotor Speed								
43.08	1.081	75.91	1.099	92.19		1.700	4.32	
47.75	1.079	68.75	1.097	83.67		1.490	3.45	
52.87	1.074	74.36	1.094	93.64		1.220	2.97	
58.14	1.069	*	1.090	*		0.912	2.28	
62.70	1.061	77.52	1.080	100.90		0.650	1.56	
67.82	1.048	82.03	1.068	116.13		0.480	0.77	
90% Design Equivalent Rotor Speed								
56.83	1.132	65.65	1.165	81.27		1.580	4.21	
60.95	1.130	68.73	1.165	86.30		1.450	3.60	
64.43	1.127	69.98	1.163	88.94		1.320	3.31	
70.31	1.118	77.34	1.157	95.97		1.040	2.63	
76.68	1.100	70.26	1.142	98.12		0.780	1.63	
83.42	1.071	67.67	1.117	109.94		0.440	0.61	

* Indicated mass-averaged temperatures behind rotor and stator were less than ambient.

Table B-1. Tabulation of Overall Performance and Percent Bleed (Continued)

Corrected Main Orifice Weight Flow $W\sqrt{\theta}/\delta$, lb_m/sec	Overall Performance						Percent Bleed
	Stage	Flow Generation Rotor			Rotor	Stator	
	\bar{P}_{2A}/P_0	η_{ad0-2A} , %	\bar{P}_2/\bar{P}_1	η_{ad1-2} , %			
100% Design Equivalent Rotor Speed							
68.98	1.156	69.38	1.204	89.42			1.29
72.87	1.154	70.48	1.205	91.33			1.52
75.89	1.148	72.13	1.201	98.63			3.06
79.79	1.137	72.69	1.193	100.68			1.21
84.71	1.116	69.46	1.174	101.85			2.71
90.04	1.088	69.30	1.147	96.45			0.57
							1.87
							0.46
							1.04
110% Design Equivalent Rotor Speed							
75.90	1.190	68.80	1.250	88.91			1.01
78.46	1.184	69.21	1.251	93.00			2.91
81.00	1.178	69.50	1.248	95.60			0.97
85.87	1.160	68.94	1.235	98.71			2.61
89.00	1.151	77.96	1.220	111.05			0.80
							2.38
							0.59
							1.82
							0.37
							1.31

Table B-2. Blade Element Performance

PERCENT DESIGN SPEED = 50.26

CORRECTED WEIGHT FLOW = 36.68

CORRECTED ROTOR SPEED = 1935.00

INLET GUIDE VANE										FLOW GENERATION ROTOR									
STATION 0 - STATION 1										STATION 1 - STATION 2									
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10		
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501								
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.000	37.200								
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	56.250	56.587	57.517	59.123	65.220								
V 0	150.12	150.12	150.12	150.12	150.12	BETA(PRI) 1	44.158	44.243	44.587	47.152	55.358								
V 1	215.64	213.87	209.81	206.26	191.31	BETA(PRI) 2	1.841	5.694	9.964	15.771	21.028								
VZ 0	150.12	150.12	150.12	150.12	150.12	V 1	215.64	213.87	209.81	206.26	191.31								
VZ 1	177.07	171.25	166.23	164.29	152.99	V 2	333.90	332.80	328.98	320.00	311.97								
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	177.07	171.25	166.23	164.29	152.99								
V-THETA 1	123.07	128.01	128.01	124.70	114.87	VZ 2	185.51	183.27	176.68	164.22	130.76								
M 0	0.1347	0.1347	0.1347	0.1347	0.1347	V-THETA 1	123.07	128.01	124.70	114.87	10.1347								
M 1	0.1939	0.1923	0.1886	0.1854	0.1719	V-THETA 2	277.63	277.80	277.51	274.65	283.24								
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	239.2	240.5	246.4	257.5	266.9								
UUBAR	0.0540	0.0216	0.0378	0.0378	0.0378	V(PRI) 2	185.6	184.2	179.4	170.6	140.1								
DFAC	-0.047	0.013	0.013	0.013	0.013	VTHETA PR1	-160.8	-168.8	-168.8	-181.9	-198.3								
EFFP	0.1999	1.0303	1.0158	1.0171	0.7879	VTHETA PR2	-6.0	-18.3	-31.0	-46.4	-50.3								
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	283.87	296.92	309.96	323.00	336.04								
DEV	7.300	6.100	6.100	7.700	8.400	U 2	283.59	296.07	308.55	321.03	332.51								
SLOTTED STATOR 3										M 1	0.1939	0.1923	0.1886	0.1854	0.1819	0.1719			
STATION 2 - STATION 2A										M 2	0.2092	0.2982	0.2946	0.2862	0.2785	0.2646			
PCT. SPAN	90	70	50	30	10	M(PRI) 1	0.2151	0.2162	0.2216	0.2315	0.2416								
BETA 2	56.250	56.587	57.517	59.123	65.220	M(PRI) 2	0.1663	0.1650	0.1607	0.1526	0.1251								
BETA 3	24.342	23.974	21.977	24.056	25.516	TURN(PK)	40.402	38.893	37.621	34.587	34.300								
V 2	33.90	33.80	32.80	32.80	31.19	UUBAR	0.0338	0.0118	0.0118	0.01248	0.2898								
V 2A	1.0675	201.84	213.45	213.18	196.91	DFAL	0.4817	0.4952	0.5293	0.6062	0.7809								
VZ 2	183.51	183.27	176.68	164.22	130.76	EFFP	0.7756	0.8064	0.8115	0.7206	0.6600								
VZ 2A	151.93	184.43	197.93	194.66	177.70	EFF	0.7740	0.8050	0.8101	0.7186	0.6575								
V-THETA 2	277.63	277.80	277.51	274.65	283.24	INCID	10.80	8.95	8.35	7.94	9.97								
V-THETA 2A	68.73	82.01	79.88	86.90	84.82	DEV	7.221	7.654	7.804	9.151	10.158								
M 2	0.2992	0.2982	0.2946	0.2862	0.2785														
M 2A	0.1495	0.1801	0.1904	0.1902	0.1755														
TURN	31.908	32.613	35.540	35.067	39.704														
UUBAR	0.2395	0.1517	0.1229	0.1102	0.1718														

Blade B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPTDU = 50.14

CORRECTED WEIGHT FLUX = 38.20

CORRECTED ROTUR SPEEDU = 1930.29

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.000	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.000	BETA 2	55.264	56.171	56.948	57.425	56.1896
V 0	156.49	156.49	156.49	156.49	156.49	BETA(PK) 1	39.727	41.694	44.882	47.844	52.367
V 1	225.99	220.84	220.99	204.70	204.70	BETA(PK) 2	2.728	5.595	10.713	14.541	23.295
V 2	156.49	156.49	156.49	156.49	156.49	V 1	225.99	224.84	220.99	217.06	204.70
VZ 0	180.04	175.09	172.90	163.70	163.70	V 2	333.24	333.64	326.97	326.00	306.66
VZ 1	185.57	180.04	175.09	172.90	163.70	VZ 1	185.57	180.04	175.09	172.90	163.70
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 2	189.88	185.74	178.33	175.52	144.46
V-THETA 1	128.97	134.69	134.83	131.24	122.91	V-THETA 1	128.97	134.69	134.83	131.24	122.91
M 0	0.1405	0.1405	0.1405	0.1405	0.1405	M 1	0.1952	0.1840	0.1840	0.1840	0.1840
M 1	0.2033	0.2022	0.1987	0.1940	0.1940	V-THETA 2	273.86	277.16	274.06	274.72	270.50
TURN	-34.80	-36.80	-37.60	-37.20	-36.00	VPR 1	241.3	241.9	247.1	257.6	268.1
UUBAR	0.0448	0.0149	0.0349	0.0497	0.0213	VPR 2	190.1	186.6	181.5	181.3	157.3
DFAC	-0.0466	0.005	0.031	0.049	0.105	VTHETA PR1	-154.2	-161.5	-174.4	-191.0	-212.3
EFFP	1.0040	1.0317	1.0140	0.9996	0.8232	VTHETA PR2	-9.0	-18.2	-33.7	-45.5	-62.2
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	283.18	286.19	309.20	322.21	335.22
DEV	7.300	6.100	6.100	7.700	8.400	U 2	282.90	295.35	307.80	310.25	332.70
						M 1	0.2033	0.2022	0.1987	0.1952	0.1840
						M 2	0.2988	0.2992	0.2931	0.2920	0.2742
						M(PK) 1	0.2176	0.2222	0.2317	0.2410	0.2410
						M(PK) 2	0.1704	0.1674	0.1627	0.1624	0.1606
						TURN(PK)	36.999	36.299	34.169	33.303	29.073
						UUBAR	0.0066	-0.0257	-0.0094	0.0233	0.1644
						UFAC	0.4516	0.4755	0.5139	0.5534	0.6795
						EFFP	0.8124	0.8684	0.8633	0.8576	0.7516
						EFF	0.8112	0.8675	0.8644	0.8565	0.7499
						INCID	8.29	6.25	5.65	5.42	7.01

STATION 2 - STATION 2A

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
BETA 2	55.264	56.171	56.948	57.425	61.896	DIA	36.299	34.169	33.303	29.073	29.073
BETA 3	24.709	22.504	20.451	25.229	26.672	UFBAR	0.0066	-0.0257	-0.0094	0.0233	0.1644
V 2	333.4	323.64	322.97	326.00	306.66	UFAC	0.4516	0.4755	0.5139	0.5534	0.6795
V 2A	163.97	201.68	216.63	218.50	203.00	EFFP	0.8124	0.8684	0.8633	0.8576	0.7516
VZ 2	189.88	185.74	178.33	175.52	144.00	EFF	0.8112	0.8675	0.8644	0.8565	0.7499
VZ 2A	148.96	186.32	202.97	197.66	181.40	INCID	8.29	6.25	5.65	5.42	7.01
V-THETA 2	273.86	271.16	274.06	274.72	270.50						
V-THETA 2A	68.54	77.19	75.69	93.13	91.12						
M 2	0.2988	0.2992	0.2931	0.2920	0.2742						
M 2A	0.1461	0.1800	0.1934	0.1910	0.1810						
TURN	30.555	33.667	36.497	32.196	35.224						
UUBAR	0.2546	0.1713	0.1188	0.1475	0.15C7						
DEV	29.35	23.14	21.09	25.87	27.31						
DIA	33.564	34.932	36.420	37.848	39.276						

DFAC	0.7650	0.6569	0.6135	0.5939	0.6265
EFFP	0.7289	0.8995	0.9201	0.9701	1.1044
INCID	-2.44	-1.53	-0.75	-0.28	4.20
LOSS PARA	-0.0702	0.6923	0.0566	0.06295	0.06567
DEV	29.35	23.14	21.09	25.87	27.31
DIA	33.564	34.932	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 50.42

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CORRECTED EDITION SCREEN = 1841 26

INLET GUIDE VANE CORRECTED KUJUK SPEED = 1941.26 FLOW GENERATION RATIO

STATION 0 - STATION 1

STATION 1 = STATION 2

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	36.598	37.600	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	54.515	56.598	56.267	56.627	59.689
V 0	164.96	164.96	164.96	164.96	164.96	BETA(PR) 1	38.146	40.218	42.946	45.873	51.485
V 1	234.27	233.42	230.76	227.27	213.84	BETA(PR) 2	3.000	4.916	10.002	14.051	21.848
V 2	164.96	164.96	164.96	164.96	164.96	V 1	234.27	233.42	230.76	227.27	213.84
VZ 1	192.37	186.91	182.83	181.03	171.01	V 2	336.82	339.97	333.00	331.08	315.000
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	192.37	186.91	182.83	181.03	171.01
V-THETA 1	133.70	139.83	140.80	137.41	128.40	VZ 2	195.52	192.08	184.92	182.12	159.000
M 0	0.1481	0.1481	0.1481	0.1481	0.1481	V-THETA 1	133.70	139.83	140.80	137.41	128.40
M 1	0.2108	0.2108	0.2100	0.2044	0.1923	V-THETA 2	274.26	280.51	276.94	276.49	271.90
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	244.6	244.58	249.8	260.0	269.8
UUBAR	0.0090	-0.0224	-0.0179	0.0	0.0179	V(PRI) 2	195.8	192.8	187.8	187.7	170.9
DFAC	-0.029	0.020	0.040	0.055	0.113	VTHETA PRI	-151.1	-170.2	-186.6	-208.0	-208.0
EFFP	1.0343	1.0675	1.0656	1.0488	0.9445	VTHETA PR2	-10.2	-16.5	-45.8	-62.6	-62.6
*****	26.9001	27.3001	27.7001	28.1001	28.1001	U 1	284.79	297.88	310.96	324.04	337.13
INCID						U 2	284.51	297.03	309.55	322.07	334.59
DEV	7.300	6.100	6.100	7.700	8.400	M 1	0.2108	0.2100	0.2076	0.2044	0.1923
						M 2	0.3021	0.3051	0.2986	0.2966	0.2818
						M(PRI) 1	0.2201	0.2202	0.2247	0.2339	0.2226
						M(PRI) 2	0.1756	0.1730	0.1684	0.1529	0.1529
						TURN(PR)	35.146	35.301	32.944	31.821	29.184
						UUBAR	0.0402	-0.0040	0.0042	0.0243	0.1248
						DFAC	0.4288	0.4535	0.4885	0.5252	0.6242
						EFFP	0.7817	0.8945	0.8397	0.8034	0.7526
						EFF	0.7803	0.8939	0.8306	0.8020	0.7508
						INCID	6.71	4.58	3.72	3.45	5.31
						DEV	8.381	6.876	7.84?	7.431	10.619
						SLUTED STATOR 3					
						STATION 2 - STATION 2A					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
BETA 2	54.515	55.598	56.627	59.689	59.689	BETA 3	24.572	21.500	19.444	24.673	27.015
BETA 3	24.572	21.500	19.444	24.673	27.015	V 2	336.82	339.97	333.00	331.08	315.06
V 2	173.05	207.38	228.38	227.14	216.11	V 2A	195.52	192.08	184.92	182.12	159.01
V 2A	195.52	192.08	184.92	182.12	159.01	VZ 2	157.93	193.28	215.36	206.40	192.52
VZ 2	274.26	280.51	276.94	276.49	271.99	V-THETA 2	72.21	75.16	76.03	94.82	98.18
V-THETA 2A						M 2	0.3021	0.3051	0.2986	0.2966	0.2818
M 2						M 2A	0.1549	0.1852	0.2041	0.2029	0.1929
M 2A						TURN	29.943	36.347	36.823	31.954	32.669
TURN						UUBAR	0.2291	0.1817	0.1028	0.1000	0.1111

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 50.11

CONNECTED WEIGHTS = 62 15

CORRECTED ROTATE SPEED = 1929.31

IN 111 GUIDE YANE FLOW GENERATION ROTOR

STATION 0 - STATION 1										STATION 1 - STATION 2									
CCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	CCT. SPAN	90	70	50	30	10	PCT. SPAN	
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501	BETA 0	0.000	0.000	0.000	0.000	0.000	0.000	
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	38.400	36.900	BETA 1	34.800	36.800	37.600	38.400	36.900	0.000	
BETA 1	34.800	36.800	37.600	38.400	39.200	BETA 2	52.991	54.485	54.537	54.537	56.885	BETA 2	52.991	54.485	54.537	54.537	56.885	0.000	
V 0	177.29	177.29	177.29	177.29	177.29	BETA(PR) 1	33.536	36.596	38.824	41.886	44.881	V 0	177.29	177.29	177.29	177.29	177.29	0.000	
V 1	253.85	248.02	247.69	246.17	239.87	BETA(PR) 2	0.983	2.871	7.733	12.583	18.658	V 1	253.85	248.02	247.69	244.17	239.87	0.000	
VZ 0	177.29	177.29	177.29	177.29	177.29	V 1	253.85	248.02	247.69	244.17	239.87	VZ 0	196.24	191.82	191.82	191.82	191.82	0.000	
VZ 1	208.45	198.60	196.24	194.49	191.82	V 2	349.57	350.57	344.56	339.08	325.35	VZ 1	208.45	198.60	196.24	194.49	191.82	0.000	
V-THETA 0	0.000	0.000	0.000	0.000	0.000	V 2	204.24	200.16	196.73	191.82	191.82	V-THETA 0	144.02	144.02	144.02	144.02	144.02	0.000	
V-THETA 1	144.88	148.57	151.13	147.63	144.02	V 2	210.42	204.24	200.16	196.73	191.82	V-THETA 1	144.88	144.88	144.88	144.88	144.88	0.000	
M 0	0.1592	0.1592	0.1592	0.1592	0.1592	V-THETA 2	144.88	144.88	144.88	144.88	144.88	M 0	0.1592	0.1592	0.1592	0.1592	0.1592	0.000	
M 1	0.2233	0.2233	0.2233	0.2198	0.2198	V-THETA 2	151.13	148.57	144.88	144.88	144.88	M 1	0.2233	0.2233	0.2233	0.2233	0.2233	0.000	
TURN	-34.80	-36.80	-37.20	-37.20	-36.90	V(PR) 1	250.1	247.4	251.9	261.2	270.7	TURN	-34.80	-36.80	-37.20	-37.20	-36.90	0.000	
UUBAR	0.0116	0.0261	0.0233	0.0349	0.0570	V(PR) 2	210.5	204.5	204.5	202.0	201.6	UUBAR	0.0116	0.0261	0.0233	0.0349	0.0570	0.000	
DFAC	-0.037	0.031	0.042	0.055	0.074	V(THETA) PR1	-138.2	-147.5	-157.9	-174.4	-187.6	DFAC	-0.037	0.031	0.042	0.055	0.074	0.000	
EFFP	1.0249	0.9772	1.0156	1.0037	0.9783	V(THETA) PR2	-3.6	-10.2	-27.2	-43.9	-60.0	EFFP	1.0249	0.9772	1.0156	1.0037	0.9783	0.000	
INCID	*****	26.9001	27.3001	27.7001	28.1001	INCID	283.04	296.14	309.04	322.05	332.53	INCID	283.04	296.14	309.04	322.05	332.53	0.000	
DEV	7.300	6.100	6.100	7.700	8.400	U 2	282.76	295.20	307.64	320.09	332.53	DEV	7.300	6.100	6.100	7.700	8.400	0.000	
SLOTTED STATOR 3										SLOTTED STATOR 3									
CCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	CCT. SPAN	90	70	50	30	10	PCT. SPAN	
BETA 2	52.991	54.370	54.485	54.537	56.885	BETA 2	0.726	0.726	0.726	0.726	0.726	BETA 2	52.991	54.370	54.485	54.537	56.885	0.000	
BETA 3	24.422	19.798	18.001	23.355	27.248	BETA 3	0.180	0.180	0.180	0.180	0.180	BETA 3	24.422	19.798	18.001	23.355	27.248	0.000	
V 2	340.57	350.59	344.56	339.08	325.35	V 2	0.0188	-0.0243	-0.0373	-0.0473	-0.0574	V 2	340.57	350.59	344.56	339.08	325.35	0.000	
V 2A	189.49	230.46	242.61	244.80	230.92	V 2A	0.0188	-0.0243	-0.0373	-0.0473	-0.0574	V 2A	189.49	230.46	242.61	244.80	230.92	0.000	
VZ 2	210.42	204.24	200.16	196.73	177.75	VZ 2	0.0188	-0.0243	-0.0373	-0.0473	-0.0574	VZ 2	210.42	204.24	200.16	196.73	177.75	0.000	
VZ 2A	172.54	216.83	230.73	224.74	205.29	VZ 2A	0.0188	-0.0243	-0.0373	-0.0473	-0.0574	VZ 2A	172.54	216.83	230.73	224.74	205.29	0.000	
V-THETA 2	279.15	284.96	280.46	276.18	272.51	V-THETA 2	78.35	78.06	74.97	105.72	144.02	V-THETA 2	279.15	284.96	280.46	276.18	272.51	0.000	
V-THETA 2A	78.35	78.06	74.97	105.72	144.02	V-THETA 2A	0.3148	0.3091	0.3041	0.2914	0.2862	V-THETA 2A	0.3148	0.3091	0.3041	0.2914	0.2862	0.000	
M 2	0.3139	0.1692	0.2061	0.2170	0.2189	M 2	0.1692	0.2061	0.2170	0.2189	0.2202	M 2	0.3139	0.1692	0.2061	0.2170	0.2189	0.000	
N 2A	28.569	34.572	36.484	31.182	29.637	N 2A	0.2443	0.1431	0.1045	0.1365	0.1365	N 2A	28.569	34.572	36.484	31.182	29.637	0.000	
UUBAR	0.2443	0.1431	0.1045	0.1365	0.1365	UUBAR	0.0188	0.0188	0.0188	0.0188	0.0188	UUBAR	0.2443	0.1431	0.1045	0.1365	0.1365	0.000	

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 50.26

CORRECTED WEIGHT FLUX = 46.75

CORRECTED ROTOR SPEED = 1935.00

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1						STATION 1 - STATION 2					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.000	BETA 2	50.963	51.021	52.077	51.058	52.826
V 0	192.54	192.54	192.54	192.54	192.54	BETA(PR) 1	30.052	31.594	34.462	37.603	42.838
V 1	271.44	272.02	268.62	265.17	250.41	BETA(PR) 2	2.416	7.161	12.138	25.168	51.138
VZ 0	192.53	192.53	192.53	192.53	192.53	V 1	271.44	272.02	268.62	265.17	250.41
VZ 1	222.90	217.81	212.82	211.21	200.25	V 2	362.45	364.09	356.27	349.80	391.69
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	222.90	212.82	211.21	212.82	211.21
V-THETA 1	154.92	162.95	163.90	160.32	150.35	VZ 2	228.28	224.55	218.96	217.00	236.68
H 0	0.1730	0.1730	0.1730	0.1730	0.1730	V-THETA 1	154.92	162.95	163.90	160.32	150.35
H 1	0.2446	0.2451	0.2450	0.2450	0.2450	V-THETA 2	281.53	286.60	281.04	274.36	312.10
TURN	-34.80	-26.80	-27.60	-37.20	-36.90	V(PR) 1	257.5	255.7	258.1	266.6	273.1
UBAR	0.0231	-0.0164	0.0033	0.0231	0.0209	V(PR) 2	228.3	224.8	220.8	222.0	237.6
DFAC	-0.021	0.021	0.043	0.055	0.110	VTHETA PR1	-129.0	-134.0	-146.1	-162.7	-185.7
EFFP	1.0093	1.0493	1.0493	1.0104	0.8136	VTHETA PR2	-2.1	-9.5	-27.5	-46.7	-21.4
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	283.87	296.92	309.96	323.00	336.04
DEV	7.300	6.100	6.100	7.700	8.400	U 2	283.59	296.07	308.55	321.03	333.51
SLOTTED STATOR 3											
BETA 2	50.963	51.921	52.077	51.658	52.826	M 1	0.3259	0.3275	0.3203	0.3143	0.3527
BETA 3	24.090	18.218	16.958	21.703	26.759	M 1(PR) 1	0.2321	0.2305	0.2326	0.2402	0.2459
V 2	362.45	364.09	356.27	349.80	391.69	M 1(PR) 2	0.2053	0.2022	0.1984	0.1994	0.2140
V 2A	221.06	243.04	264.10	265.36	239.14	TURN(PR)	29.534	29.178	27.300	25.465	37.670
VZ 2	228.28	224.55	218.96	217.00	236.68	UUBAR	0.0629	0.0099	-0.0063	-0.1171	0.2255
VZ 2A	201.81	230.86	252.62	246.55	213.53	DFAC	0.2466	0.2420	0.2289	0.2255	0.2289
V-THETA 2	281.53	285.60	281.04	274.36	312.10	EFFP	0.8023	0.8006	0.8746	0.8619	1.3284
V-THETA 2A	9C.23	75.98	77.03	98.13	107.67	EFF	0.8012	0.8899	0.8739	0.8610	1.3315
H 2	C.3259	0.3275	0.3203	0.3143	0.3527	INCID	-1.39	-4.05	-4.77	-4.82	-2.52
H 2A	0.1977	0.2177	0.2367	0.2377	0.2339	DEV	5.898	4.376	5.001	5.518	-5.702
TURN	26.873	33.703	35.119	29.955	26.067						
UBAR	0.2098	0.1752	0.0876	0.0859	0.3975						

DFAC	0.6103	0.5847	0.6192	0.4803	0.6468
EFFP	0.8261	0.9836	1.2852	1.1156	0.4217
INCID	-6.74	-5.78	-5.62	-6.04	-4.87
LOSS PARA	.08037	.07280	.03813	.03762	.17306
DEV	24.73	18.86	17.60	22.34	27.40
DIA	33.564	34.992	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 70.01

CORRECTED WEIGHT FLUW = 43.08

CORRECTED ROTUR SPEED = 2695.51

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	UIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	57.880	60.010	62.271	66.196	73.760
V 0	177.01	177.01	177.01	177.01	177.01	177.C1	51.605	53.632	56.072	61.715	61.715
V 1	246.09	245.50	245.27	241.50	238.35	BETA(PR) 2	2.1504	3.501	8.156	15.004	28.037
VZ 0	177.01	177.01	177.01	177.01	177.01	V 1	246.09	245.27	241.50	238.67	224.35
VZ 1	202.07	196.39	191.33	190.10	179.41	V 2	458.89	459.95	451.56	436.91	418.91
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	202.07	196.39	191.33	190.10	179.41
V-THETA 1	140.44	146.92	147.35	144.30	134.70	VZ 2	243.99	229.91	210.11	176.34	117.15
M 0	0.1590	0.1590	0.1590	0.1590	0.1590	V-THETA 1	140.44	146.92	147.35	144.30	134.70
M 1	0.2215	0.2208	0.2174	0.2148	0.2018	V-THETA 2	388.65	398.37	399.71	402.40	402.40
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	W(PRI) 1	325.4	331.2	342.8	359.9	378.6
UBAR	0.1362	-0.1634	-0.1439	-0.1401	0.0389	W(PK) 2	244.1	230.3	212.3	182.6	132.7
DFAC	-0.0007	0.040	0.064	0.075	0.133	V(PRI) PR1	-266.7	-284.4	-305.6	-333.4	-333.4
EFP	1.2157	1.2624	1.2500	1.2588	1.2998	V(THETA) PR2	-6.4	-14.1	-30.1	-47.5	-62.4
INCID	*****	26.3001	27.3001	27.7001	28.0001	U 1	395.44	413.61	431.78	449.94	468.11
DEV	7.360	6.100	6.100	7.700	8.400	U 2	395.05	412.44	429.82	447.20	464.59
						M 1	0.2215	0.2148	0.2174	0.2208	0.2118
						M 2	0.4106	0.4118	0.4037	0.3899	0.3725
						M(PRI) 1	0.2929	0.2981	0.3085	0.3239	0.3406
						M(PRI) 2	0.2184	0.2062	0.1897	0.1629	0.1180
						TURN(PR)	50.102	50.130	47.915	43.055	33.618
						UBAR	0.2775	0.2974	0.3543	0.4526	0.5671
						QFAC	0.5539	0.6226	0.7044	0.8193	0.9692
						EFFP	0.7433	0.8048	0.7659	0.7142	0.6348
						EFF	0.7399	0.8020	0.7627	0.7103	0.6299
						INCID	20.17	17.99	16.84	15.70	16.35
						DEV	6.884	5.461	5.996	8.444	17.16
BETA 2	57.880	60.010	62.271	66.196	73.760						
BETA 3	28.041	28.564	26.970	26.902	21.296						
V 2	458.89	459.89	451.56	436.91	418.91						
V 2A	168.08	265.31	281.32	280.52	246.70						
VZ 2	243.99	229.91	210.11	176.34	117.15						
VZ 2A	166.00	233.02	250.72	250.16	227.99						
V-THETA 2	388.65	396.37	399.71	399.74	402.20						
V-THETA 2A	88.42	126.86	127.59	126.93	88.87						
M 2	0.4106	0.4118	0.4037	0.3899	0.3725						
M 2A	0.1676	0.2353	0.2496	0.2488	0.2168						
TURN	29.839	31.446	35.301	39.294	52.464						
UBAR	0.3062	0.1772	0.1328	0.1080	0.1724						

DFAC	0.8631	0.6806	0.6513	0.6539	0.7842
EFFP	2.1057	0.8880	1.0439	1.1833	1.238
INCID	0.18	2.31	4.57	8.50	16.06
LOSS PARA	.11340	.06812	.07417	.05453	.08288
DEV	28.68	29.20	27.61	27.54	21.94
DI	33.564	34.992	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 69.90

CORRECTED WEIGHT FLOW = 52.78

CORRECTED ROTUR SPEED = 2690.97

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	55.314	56.585	57.398	57.200	56.848
V 0	218.25	219.25	218.25	218.25	218.25	BETA(PR) 1	50.963	52.874	55.496	57.610	62.269
V 1	249.32	249.23	244.53	241.47	220.27	BETA(PR) 2	3.895	7.120	11.072	15.845	23.162
VZ 0	218.25	218.25	218.25	218.25	218.25	V 1	249.32	249.23	244.53	241.47	220.27
VZ 1	204.73	199.56	199.74	192.34	176.15	V 2	458.04	459.76	455.8	448.53	428.04
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	204.73	199.56	193.74	192.34	176.15
V-THETA 1	142.29	149.29	149.20	145.99	132.26	VZ 2	260.66	259.85	250.44	241.67	201.96
M 0	0.1963	0.1963	0.1963	0.1963	0.1963	V-THETA 1	142.29	149.29	149.20	145.99	132.26
M 1	0.2245	0.2244	0.2201	0.2173	0.1981	V-THETA 2	376.64	379.29	380.09	377.86	377.40
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	325.1	330.6	339.1	359.1	378.5
UUBAR	0.0180	-0.0462	-0.0257	-0.0231	0.1567	V(PRI) 2	261.3	261.9	255.2	251.2	219.7
DFAC	0.172	0.209	0.231	0.241	0.310	V(THETA) PRI	-252.5	-263.6	-281.9	-303.2	-335.1
EFFP	1.1484	1.2718	1.2186	1.2370	0.2531	V(THETA) PR2	-17.7	-32.5	-49.0	-68.6	-86.4
INC10	*****	26.9001	27.3001	27.7001	28.1001	U 1	394.78	412.91	431.05	449.19	467.32
DEV	7.300	6.100	6.100	7.700	8.400	U 2	394.39	411.74	429.10	446.45	463.80
						M 1	0.2245	0.2244	0.2201	0.2173	0.1981
						M 2	0.4102	0.4125	0.4012	0.3815	
						M(PK) 1	0.2927	0.2977	0.3079	0.3232	0.3404
						M(PK) 2	0.2340	0.2349	0.2285	0.2247	0.1958
						TURN(PK)	47.068	45.755	44.424	41.765	39.106
						UUBAR	0.3143	0.2623	0.2767	0.3018	0.4251
						DFAC	0.4837	0.4996	0.5509	0.5981	0.7318
						EFFP	0.7135	0.8387	0.7638	0.7686	0.6813
						EFF	0.7101	0.8367	0.7809	0.7654	0.6831
						INC10	19.52	17.23	16.27	15.19	16.41
						DEV	9.275	9.080	8.912	9.225	

PCT. SPAN	90	70	50	30	10	
BETA 2	55.314	55.585	56.619	57.398	61.848	
BETA 3	25.547	22.600	20.589	24.946	25.375	
V 2	458.04	459.76	455.18	448.53	428.04	
V 2A	229.64	289.41	303.40	317.05	288.45	
VZ 2	260.66	259.85	250.44	241.67	201.96	
VZ 2A	207.19	267.18	284.02	287.48	260.62	
V-THETA 2	376.64	379.29	380.09	377.86	377.40	
V-THETA 2A	99.03	111.22	106.69	133.72	123.61	
M 2	0.4102	0.4125	0.4076	0.4012	0.3815	
M 2A	0.2036	0.2575	0.2700	0.2823	0.2566	
TURN	29.767	32.985	36.030	32.452	36.473	
UUBAR	0.2676	0.1637	0.1434	0.1139	0.1622	

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 68.97

CORRECTED WEIGHT FLOW = 58.14

CORRECTED ROTOR SPEED = 2655.22

		INLET GUIDE VANE				STATION 0 - STATION 1				STATION 1 - STATION 2				FLOW GENERATION ROTOR			
PCT.	SPAN	90	70	50	30	10	PCT.	SPAN	90	70	50	30	10	PCT.	SPAN		
DIA	33.622	35.167	36.711	38.226	39.801	DIA	33.589	35.067	36.445	38.023	39.001	39.001	39.001	39.001	39.001	39.001	
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.700	36.900	36.900	36.900	36.900	36.900	36.900	
BETA 1	34.800	36.800	37.600	37.209	36.900	BETA 2	53.713	54.785	55.556	55.191	58.616	58.616	58.616	58.616	58.616	58.616	
V 0	241.40	241.40	241.40	241.40	241.40	BETA(PR) 1	34.896	36.823	39.859	42.751	47.546	47.546	47.546	47.546	47.546	47.546	
V 1	340.66	339.94	339.47	330.53	312.72	BETA(PR) 2	34.985	35.975	8.745	13.372	19.249	19.249	19.249	19.249	19.249	19.249	
VZ 0	241.40	241.40	241.40	241.40	241.40	V 1	340.66	339.94	334.47	330.53	312.72	312.72	312.72	312.72	312.72	312.72	
VZ 1	279.73	272.20	265.00	263.28	250.08	V 2	467.87	474.03	465.59	460.43	441.90	441.90	441.90	441.90	441.90	441.90	
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	279.73	272.20	265.00	263.28	250.08	250.08	250.08	250.08	250.08	250.08	
V-THETA 1	194.42	203.63	204.08	199.84	187.76	VZ 2	276.50	273.35	265.35	262.83	230.00	230.00	230.00	230.00	230.00	230.00	
M 0	0.2172	0.2172	0.2172	0.2172	0.2172	V-THETA 1	194.42	203.63	204.08	199.84	187.76	187.76	187.76	187.76	187.76	187.76	
M 1	0.3081	0.3074	0.3074	0.3074	0.3074	V-THETA 2	377.13	387.28	382.98	378.04	377.33	377.33	377.33	377.33	377.33	377.33	
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	341.1	340.0	345.2	358.5	370.5	370.5	370.5	370.5	370.5	370.5	
UUBAR	0.0379	-0.0673	-0.0379	-0.0273	0.1367	V(PR) 2	277.2	274.0	268.5	270.2	244.6	244.6	244.6	244.6	244.6	244.6	
DFAC	-0.022	0.025	0.049	0.061	0.114	VTHETA PR1	-195.1	-203.8	-221.2	-243.4	-274.4	-274.4	-274.4	-274.4	-274.4	-274.4	
EFFP	1.0600	1.3937	1.0648	1.0555	0.8605	VTHETA PR2	-12.0	-19.0	-40.8	-62.5	-80.3	-80.3	-80.3	-80.3	-80.3	-80.3	
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	389.53	407.43	425.32	443.22	461.11	461.11	461.11	461.11	461.11	461.11	
DEV	7.300	6.100	6.100	7.700	8.400	U 2	389.15	406.27	423.40	440.52	457.64	457.64	457.64	457.64	457.64	457.64	
		SLOTTED STATOR 3				M 1	0.3081	0.3074	0.2987	0.2824	0.2824	0.2824	0.2824	0.2824	0.2824	0.2824	0.2824
		STATION 2 - STATION 2A				M 2	0.4280	0.4322	0.4240	0.4190	0.4190	0.4190	0.4190	0.4190	0.4190	0.4190	0.4190
		STATION 2 - STATION 2A				MIPR 1	0.3084	0.3075	0.3121	0.3145	0.3145	0.3145	0.3145	0.3145	0.3145	0.3145	0.3145
		STATION 2 - STATION 2A				MIPR 2	0.2523	0.2498	0.2445	0.2459	0.2459	0.2459	0.2459	0.2459	0.2459	0.2459	0.2459
		STATION 2 - STATION 2A				TURN(PR)	32.411	32.848	31.114	29.379	28.297	28.297	28.297	28.297	28.297	28.297	28.297
		STATION 2 - STATION 2A				UUBAR	0.0387	-0.0192	-0.0263	-0.0143	-0.1035	-0.1035	-0.1035	-0.1035	-0.1035	-0.1035	-0.1035
		STATION 2 - STATION 2A				DFAC	0.4010	0.4209	0.4504	0.4765	0.501	0.501	0.501	0.501	0.501	0.501	0.501
		STATION 2 - STATION 2A				EFFP	6.8859	17.7649	10.5006	8.5633	4.2052	4.2052	4.2052	4.2052	4.2052	4.2052	4.2052
		STATION 2 - STATION 2A				EFF	6.9318	17.9732	10.6205	8.6618	4.2472	4.2472	4.2472	4.2472	4.2472	4.2472	4.2472
		STATION 2 - STATION 2A				INCLU	3.46	1.18	0.63	0.33	2.19	2.19	2.19	2.19	2.19	2.19	2.19
		STATION 2 - STATION 2A				UEV	7.865	5.935	6.585	6.752	8.379	8.379	8.379	8.379	8.379	8.379	8.379
		STATION 2 - STATION 2A				BETA 2	53.713	54.785	55.256	55.191	58.636	58.636	58.636	58.636	58.636	58.636	58.636
		STATION 2 - STATION 2A				BETA 1	25.534	25.875	26.856	26.752	26.988	26.988	26.988	26.988	26.988	26.988	26.988
		STATION 2 - STATION 2A				V 2	467.87	474.03	465.59	460.43	441.90	441.90	441.90	441.90	441.90	441.90	441.90
		STATION 2 - STATION 2A				V 2A	256.07	307.88	326.46	338.06	314.85	314.85	314.85	314.85	314.85	314.85	314.85
		STATION 2 - STATION 2A				VZ 2	273.90	273.35	265.35	262.35	230.00	230.00	230.00	230.00	230.00	230.00	230.00
		STATION 2 - STATION 2A				VZ 2A	236.87	287.71	309.13	309.13	280.57	280.57	280.57	280.57	280.57	280.57	280.57
		STATION 2 - STATION 2A				V-THETA 2	377.13	387.28	382.58	378.44	377.33	377.33	377.33	377.33	377.33	377.33	377.33
		STATION 2 - STATION 2A				V-THETA 2A	110.78	109.61	104.95	136.83	142.88	142.88	142.88	142.88	142.88	142.88	142.88
		STATION 2 - STATION 2A				M 2	0.4260	0.4322	0.4240	0.4190	0.4009	0.3972	0.3972	0.3972	0.3972	0.3972	0.3972
		STATION 2 - STATION 2A				M 2A	0.308	0.2786	0.2953	0.3059	0.2844	0.2844	0.2844	0.2844	0.2844	0.2844	0.2844
		STATION 2 - STATION 2A				TURN	28.079	33.929	36.504	31.316	31.648	31.648	31.648	31.648	31.648	31.648	31.648
		STATION 2 - STATION 2A				UUBAR	0.2551	0.1804	0.1312	0.1124	0.1536	0.1536	0.1536	0.1536	0.1536	0.1536	0.1536
		STATION 2 - STATION 2A				DFAC	0.6902	0.6059	0.5701	0.5142	0.5493	0.5493	0.5493	0.5493	0.5493	0.5493	0.5493
		STATION 2 - STATION 2A				EFFP	0.1160	0.9709	1.0294	1.1003	1.2199	1.2199	1.2199	1.2199	1.2199	1.2199	1.2199
		STATION 2 - STATION 2A				INCID	-3.99	-2.91	-2.44	-2.51	0.94	0.94	0.94	0.94	0.94	0.94	0.94
		STATION 2 - STATION 2A				LOSS PARA	.09650	.07377	.06554	.04851	.06675	.06675	.06675	.06675	.06675	.06675	.06675
		STATION 2 - STATION 2A				DEV	33.564	34.992	36.420	37.848	39.276	39.276	39.276	39.276	39.276	39.276	39.276
		STATION 2 - STATION 2A				DIA											

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 59.84

CORRECTED WEIGHT FLOW = 52.70

CORRECTED ROTOR SPEED = 2688.95

INLET GUIDE VANE

PCT. SPAN	STATION 0 - STATION 1				STATION 1 - STATION 2				FLOW GENERATION ROTOR		
	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.712	38.256	39.401	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	38.400	39.200	BETA 2	51.482	52.328	52.430	51.712	51.900
V 0	261.33	261.33	261.33	261.33	261.33	BETA(PR) 1	31.133	32.817	35.749	38.891	43.900
V 1	369.82	369.92	364.87	359.91	340.86	BETA(PR) 2	1.190	3.288	7.925	12.414	19.225
VZ 0	261.33	261.33	261.33	261.33	261.33	V 1	369.82	369.92	369.91	340.86	340.86
VZ 1	303.67	296.20	289.08	286.68	272.58	V 2	495.50	497.17	488.30	481.34	457.76
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	303.67	296.20	289.08	286.68	272.58
V-THETA 1	211.06	221.59	222.62	217.60	204.65	VZ 2	304.18	297.26	293.49	279.92	270.92
M 0	0.2354	0.3354	0.2354	0.2354	0.2354	V-THETA 1	211.06	221.59	222.62	204.65	204.65
M 1	0.3350	0.3351	0.3304	0.3258	0.3082	V-THETA 2	307.68	303.96	307.39	381.51	369.98
TURN	-34.80	-37.80	-37.60	-37.20	-36.30	V(PR) 1	354.8	352.5	356.2	368.3	378.3
UUBAR	0.0414	-0.0755	-0.0522	-0.0306	0.1365	V(PR) 2	308.6	306.7	306.1	300.45	286.9
DFAC	-0.0332	0.020	0.042	0.055	0.108	VTHETA PR1	-183.4	-191.0	-208.1	-231.2	-262.3
EFFP	1.0597	1.0972	1.0755	1.0541	0.9555	VTHETA PR2	-6.4	-17.5	-41.4	-66.6	-94.5
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	394.48	412.60	430.73	448.85	466.97
DEV	7.300	6.100	6.100	7.700	8.400	U 2	394.09	411.43	428.77	446.11	463.46
						M 1	0.3350	0.3351	0.3304	0.3258	0.3082
						M 2	0.4469	0.4402	0.4337	0.4115	
						MIPR1 1	0.3214	0.3193	0.3226	0.3334	
						MIPR1 2	0.2784	0.2750	0.2706	0.2708	
						TURN(PR)	29.943	29.330	27.623	26.477	
						UIBAR	0.0767	0.0211	0.0053	0.0137	
						DFAC	0.3286	0.3049	0.3617	0.3904	
						EFFP	0.8058	0.8969	0.8802	0.8159	
						FFF	0.8038	0.8957	0.8789	0.9149	
						INCID	-0.31	-2.82	-3.48	-3.53	
						DEV	6.570	5.248	5.766	5.794	8.355
BETA 2	51.482	52.328	52.499	52.430	53.712						
BETA 3	26.000	18.200	18.000	20.400	29.500						
V 2	495.50	497.72	488.30	457.76	372.68						
V 2A	302.43	348.77	369.46	372.35	332.68						
VZ 2	308.58	304.18	297.26	293.49	270.92						
VZ 2A	271.82	331.32	351.38	349.00	289.55						
V-THETA 2	387.68	393.96	387.39	381.51	366.98						
V-THETA 2A	132.58	108.93	114.17	129.79	163.82						
M 2	0.4469	0.4492	0.4402	0.4337	0.4115						
M 2A	0.2699	0.3124	0.3311	0.3335	0.2971						
TURN	25.482	34.128	34.499	32.030	24.212						
UUBAR	0.2354	0.1520	0.0877	0.0900	0.1693						
DFAC	0.6045	0.5490	0.4980	0.4744	0.4946						
EFFP	0.7479	0.9521	1.0942	0.9684	0.8897						
INCID	-6.22	-5.37	-5.20	-5.27	-3.99						
LOSS PARA	0.08872	0.06325	0.03831	0.03979	0.07183						
DEV	26.64	18.84	18.64	21.04	30.14						
DIA	33.564	34.992	36.420	37.848	39.276						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 69.96

CORRECTED WEIGHT FLUX = 67.82

CORRECTED ROTOR SPEED = 2693.46

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	STATION 1 - STATION 2
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501	
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	36.800	37.600	37.600	37.600	37.600	
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	49.605	49.959	50.366	49.632	50.201	
V 0	284.02	284.02	284.02	284.02	284.02	V 0	284.02	284.02	284.02	284.02	284.02	
V 1	407.73	406.60	406.83	394.22	373.77	V 1	25.882	27.534	30.476	32.932	39.149	
VZ 0	284.02	284.02	284.02	284.02	284.02	VZ 0	284.02	284.02	284.02	284.02	284.02	
VZ 1	334.81	325.58	317.58	314.01	298.90	VZ 1	407.73	406.60	400.83	394.22	373.77	
V-THETA 0	0.00	0.00	0.00	0.00	0.00	V-THETA 0	510.53	511.51	506.32	496.29	477.83	
V-THETA 1	232.70	244.57	238.34	224.42	VZ 2	334.81	325.58	317.58	314.01	298.90		
H 0	0.2561	0.2561	0.2561	0.2561	0.2561	VZ 2	330.85	332.93	322.97	321.44	305.86	
H 1	0.3702	0.3692	0.3638	0.3576	0.3387	V-THETA 1	232.70	243.57	244.57	238.34	224.42	
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V-THETA 2	388.82	396.20	389.94	378.12	367.11	
UUBAR	0.021	-0.0672	-0.0519	-0.0305	0.1252	V(PK) 1	372.1	367.2	368.5	378.5	385.4	
DFAC	-0.040	0.008	0.032	0.048	0.100	V(PK) 2	330.9	333.3	325.4	328.7	320.9	
EFFP	1.0442	1.0805	1.0687	1.0491	0.8750	VTHETA PR1	-162.4	-169.7	-186.9	-211.3	-243.3	
INC1D	*****	26.9001	27.5001	27.7001	28.1001	VTHETA PR2	1.027	-15.9	-39.6	-68.7	-91.1	
DEV	7.300	6.100	6.100	7.700	8.400	U 1	395.14	413.30	431.45	449.60	467.15	
						U 2	394.75	412.12	429.49	446.86	464.23	
						M 1	0.3702	0.3692	0.3638	0.3576	0.3387	
						M 2	0.4614	0.4684	0.4580	0.4482	0.4299	
						M(PK) 1	0.3379	0.3334	0.3344	0.3433	0.3492	
						M(PK) 2	0.2991	0.3017	0.2968	0.2887		
						TURN(PR)	24.855	24.796	23.493	21.862	21.532	
						UUBAK	0.1074	0.0225	0.0223	0.0184	0.0508	
						UFAC	0.2782	0.2669	0.2915	0.3032	0.3481	
						EFFP	0.7151	0.8692	0.8942	0.8389	0.7277	
						EFF	0.7126	0.8679	0.8932	0.8373	0.7250	
						INC1D	-5.56	-8.11	-8.75	-8.49	-6.21	
						UEV	6.407	4.698	4.823	5.451	6.747	
BETA 2	49.605	49.959	50.366	49.632	50.201							
BETA 3	24.632	17.495	17.484	22.315	28.826							
V 2	510.53	517.51	508.32	496.29	477.83							
V 2A	341.34	393.25	405.68	409.73	366.03							
VZ 2	330.85	332.93	322.97	321.44	305.86							
VZ 2A	310.48	310.06	389.94	379.05	320.68							
V-THETA 2	388.82	395.20	389.94	378.12	367.11							
V-THETA 3	142.27	118.22	121.38	155.57	176.48							
H 2	0.4614	0.4684	0.4580	0.4482	0.4299							
H 2A	0.3062	0.3543	0.3553	0.3588	0.3281							
TURN	24.973	32.464	32.982	27.317	21.375							
UUBAK	0.2281	0.1344	0.0890	0.0705	0.1872							
DFAC	0.5329	0.4744	0.4397	0.3872	0.4312							
EFFP	0.9272	1.3801	1.2771	1.5340	1.1503							
INC1D	-8.10	-7.74	-7.33	-8.07	-7.50							
LOSS PARA	08699	.05607	.03864	.03077	.07994							
DEV	25.27	18.14	18.12	22.96	29.47							
DIA	33.564	34.992	36.420	37.848	39.276							

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 89.69

CORRECTED WEIGHT FLUX = 56.83

CORRECTED ROTOR SPEED = 3453.23

INLET GUIDE VANE

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.067	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	57.146	58.869	60.930	64.817	72.411
V 0	235.71	235.71	235.71	235.71	235.71	BETA(PR) 1	49.355	52.674	53.966	56.218	60.154
V 1	331.72	321.31	321.09	300.73	235.71	BETA(PR) 2	2.400	5.768	8.902	14.955	25.110
VZ 0	235.71	235.71	235.71	235.71	235.71	V 1	331.72	321.31	321.52	321.09	300.73
VZ 1	272.39	257.28	257.90	255.75	240.49	V 2	58.59	58.59	58.59	58.59	58.59
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	272.39	257.28	257.90	257.57	240.49
V-THETA 1	189.31	192.47	198.61	194.13	180.56	VZ 2	318.22	300.78	281.59	279.33	164.27
M 0	0.2121	0.2121	0.2121	0.2121	0.2121	V-THETA 1	189.31	192.47	198.61	194.13	180.56
M 1	0.2998	0.2903	0.2941	0.2900	0.2714	V-THETA 2	492.77	497.99	506.54	508.99	518.20
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	418.2	424.3	438.4	460.0	483.2
UUBAR	0.0573	-0.0504	-0.0662	-0.0551	0.1367	V(PR) 2	318.5	302.3	285.0	247.7	181.4
DFAC	-0.019	0.053	0.066	0.127	VTHETA PR1	-317.3	-337.4	-354.5	-382.3	-419.1	
EFFP	1.0835	1.1423	1.1017	1.0936	0.8523	VTHETA PR2	-13.3	-30.4	-44.1	-63.9	-77.0
INCID	***	26.9001	27.3001	27.7001	28.1001	U 1	506.61	529.88	553.15	576.43	599.70
DEV	7.300	6.100	6.100	7.700	8.400	U 2	506.10	528.37	550.64	572.91	595.18

SLOTTED STATOR 3

STATION 2 - STATION 2A

PCT. SPAN	90	70	50	30	10	DIA	1.780	7.728	6.742	8.335	14.240
BETA 2	57.146	58.869	60.930	64.817	72.411	M(PR) 1	0.5257	0.5215	0.5178	0.5014	0.4819
BETA 3	26.178	27.305	25.447	20.919	543.61	M(PR) 2	0.3780	0.3833	0.3961	0.4155	0.4361
V 2	586.59	581.78	579.55	562.44	533.19	TURB(PR)	46.954	46.906	45.065	41.262	35.044
V 2A	241.57	345.16	359.54	368.70	33.19	UUBAR	0.2027	0.2519	0.2731	0.2871	0.5236
VZ 2	318.22	300.78	281.59	239.33	164.27	DFAC	0.5276	0.5833	0.6588	0.7767	0.9607
VZ 2A	26.179	30.670	324.66	332.56	314.96	EFFP	0.8045	0.8416	0.7832	0.7455	0.6642
V-THETA 2	492.77	497.99	506.94	508.99	518.20	INCID	0.8003	0.8382	0.7783	0.7399	0.6567
V-THETA 2A	106.57	158.33	154.49	159.19	120.39	DEV	17.91	17.03	14.74	13.80	14.79
M 2	0.5257	0.5215	0.5178	0.5014	0.4819						
M 2A	0.2115	0.3040	0.3167	0.3247	0.2966						
TURN	30.968	31.564	35.483	39.237	51.492						
UUBAR	0.3271	0.1626	0.1524	0.1064	0.1475						

DFAC	0.8628	0.6614	0.6561	0.6393	0.7402
EFFP	0.6102	0.7591	0.8793	0.9724	1.3961
INCID	-0.55	1.17	3.23	7.12	14.71
LOSS PARA	.12311	.06320	.06262	.04530	.06714
DEV	26.82	27.95	26.09	26.22	21.56
DIA	33.564	34.992	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 90.17

CORRECTED WEIGHT FLW = 60.95

CORRECTED ROTUR SPEED = 3471.71

INLET GUIDE VANE

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	38.900	39.800	BETA 2	56.544	57.473	58.984	61.392	69.302
V 0	253.65	253.65	253.65	253.65	253.65	BETAPR 1	46.131	47.898	50.516	53.032	57.090
V 1	351.43	351.69	353.80	344.50	328.37	BETAPR 2	3.167	6.746	10.618	15.167	23.504
VZ 0	253.65	253.65	253.65	253.65	253.65	V 1	357.43	353.69	348.50	328.37	328.37
VZ 1	291.51	287.22	280.31	277.59	262.59	V 2	588.35	585.84	580.52	571.57	549.69
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	293.51	287.22	280.31	277.59	262.59
V-THETA 1	203.99	214.86	215.87	210.70	197.16	VZ 2	324.35	315.00	299.13	273.68	188.89
H 0	0.2284	0.2284	0.2284	0.2284	0.2284	V-THETA 1	203.99	214.86	215.87	210.70	197.16
H 1	0.3235	0.3247	0.3247	0.3202	0.3153	V-THETA 2	490.86	493.94	497.51	501.79	516.22
TURN	-3.80	-3.680	-3.76.60	-3.7.20	-36.90	VIPK 1	423.5	428.4	440.8	461.6	483.3
UBAR	0.0038	-0.0572	-0.0401	-0.0191	0.1603	VIPK 2	324.9	317.2	304.3	283.6	206.0
DFAC	-0.021	0.021	0.043	0.058	0.114	VTHETA PR1	-305.3	-317.8	-340.2	-368.8	-405.3
EFFP	1.0225	1.0783	1.0632	1.0425	0.8343	VTHETA PR2	-17.9	-37.3	-56.1	-74.2	-82.1
INCID	*****	26.9001	27.3001	27.1001	28.1001	U 1	509.32	532.71	556.11	579.51	602.91
DEV	7.300	6.100	6.100	7.700	8.400	U 2	531.20	553.59	575.98	598.37	
						M 1	0.3235	0.347	0.3202	0.3153	0.2967
						M 2	0.5286	0.5268	0.5210	0.5116	0.4891
						M (PR) 1	0.3834	0.3878	0.3989	0.4176	0.4468
						M (PR) 2	0.2919	0.2852	0.2731	0.2538	0.1833
						TURN(PR)	42.963	41.153	39.898	37.866	33.585
						UBAR	0.1245	0.1166	0.1606	0.1424	
						DFAC	0.5030	0.5328	0.5909	0.6765	0.8917
						EFFP	0.8697	0.9332	0.8974	0.8459	0.7798
						EFF	0.8670	0.9317	0.8951	0.8425	0.7238
						INCID	14.69	12.26	11.29	10.61	11.73
						DEV	8.547	8.706	8.458	8.547	12.634

STATION 2 - STATION 2A

PCT. SPAN	90	70	50	30	10						
BETA 2	56.544	57.473	58.984	61.392	69.902	EFFP	0.8697	0.9332	0.8974	0.8459	0.7798
BETA 3	25.959	25.621	22.981	26.084	22.350	EFF	0.8670	0.9317	0.8951	0.8425	0.7238
V 2	588.35	585.84	580.52	571.57	549.69	INCID	14.69	12.26	11.29	10.61	11.73
V 2A	261.57	358.61	365.28	387.44	341.79	DEV	8.547	8.706	8.458	8.547	12.634
VZ 2	324.35	315.35	299.13	273.68	188.89						
VZ 2A	235.18	323.35	316.29	347.98	316.11						
V-THETA 2	490.86	493.94	497.51	501.79	516.22						
V-THETA 2A	114.50	155.07	142.62	170.35	129.97						
H 2	0.5286	0.5268	0.5210	0.5116	0.4891						
H 2A	0.2295	0.3167	0.3226	0.3423	0.3009						
TURN	30.585	31.852	36.003	35.08	47.552						
UBAR	0.3180	0.1616	0.1582	0.1042	0.1695						

DFAC	0.6223	0.6402	0.6489	0.5971	0.7244
EFFP	0.5835	0.7278	0.7594	0.8897	0.9979
INCID	-1.16	-0.23	1.28	3.69	12.20
LOSS PARA	.11999	.06374	.06630	.04417	.07642
DEV	26.60	26.26	23.62	26.72	22.99
0IA	33.564	34.992	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPTED = 90.16

CONNECTED WEIGHTS Obj = 64 43

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Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 89.86

CORRECTED WEIGHT FLOW = 70.31

CORRECTED ROTOR SPE_TD = 3459.53

STATION 0 - STATION 1										STATION 1 - STATION 2									
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10		
DIA	33.622	35.167	36.711	38.256	39.801	OIA	33.589	35.067	36.545	38.023	39.501	BETA 1	34.800	36.800	37.600	37.200	36.900		
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 2	54.373	55.696	55.812	56.690	59.530	BETA 1	34.800	36.800	37.600	37.200	36.900		
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	54.373	55.696	55.812	56.690	59.530	BETA 1	34.800	36.800	37.600	37.200	36.900		
V 0	295.21	295.21	295.21	295.21	295.21	BETA(PRI)	1	36.549	38.542	41.554	44.735	49.416	V 1	430.42	429.17	429.17	422.24	414.32	
V 1	430.32	429.17	422.24	414.32	391.66	BETA(PRI)	2	2.050	4.985	9.722	13.853	19.951	V 2	430.32	429.17	429.17	422.24	414.32	
VZ 0	295.20	295.20	295.20	295.20	295.20	V 1	430.32	429.17	429.17	422.24	414.32	VZ 1	330.02	313.21	313.21	304.53	291.66		
VZ 1	353.36	343.65	334.53	330.02	313.21	V 2	601.57	604.81	597.37	591.01	570.07	V-THETA 0	0.00	0.00	0.00	0.00	0.00		
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	353.36	343.65	334.53	330.02	313.21	V-THETA 1	250.50	235.16	230.50	225.00	219.00		
V-THETA 1	245.59	257.08	257.63	250.50	235.16	VZ 2	350.42	340.86	335.67	324.57	289.07	V-THETA 1	250.50	235.16	230.50	225.00	219.00		
M 0	0.2663	0.2663	0.2663	0.2663	0.2663	V-THETA 2	245.59	257.08	257.63	250.50	235.16	M 1	0.3903	0.3838	0.3764	0.3690	0.3614		
M 1	0.3914	0.3903	0.3838	0.3764	0.3690	V-THETA 1	488.97	499.61	499.61	494.14	493.92	V-THETA 2	0.4543	0.4543	0.4543	0.4543	0.4543		
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	430.9	439.4	439.4	447.0	464.6	TURN	-0.0057	-0.0184	-0.0127	-0.0182	-0.0182		
UUBAR	0.0057	-0.0184	-0.0127	-0.0182	-0.0182	V(PR) 2	350.9	342.2	340.6	334.3	307.5	UUBAR	-0.0182	-0.0182	-0.0182	-0.0182	-0.0182		
DFAC	-0.056	-0.007	0.017	0.0317	0.0317	V(PR) 1	-261.9	-273.8	-296.8	-327.0	-356.6	EFFP	1.0506	1.0303	1.0013	0.8260	0.7663		
EFFP	1.0169	1.0506	1.0303	1.0013	0.8260	V(PR) 2	-10.1	-29.7	-57.5	-80.0	-104.9	INCID	26.9001	27.3001	27.7001	28.1001	28.1001		
INCID	*****	*****	*****	*****	*****	U 1	507.53	530.85	554.16	577.48	600.79	DEV	7.300	6.100	6.100	7.700	8.400		
DEV	7.300	6.100	6.100	7.700	8.400	M 1	507.53	529.34	551.65	573.96	598.26	SLOTTED STATOR 3	0.3114	0.3093	0.3083	0.3076	0.3069		
M 2	0.5443	0.5484	0.5484	0.5484	0.5484	M 1	0.4060	0.3995	0.4060	0.4220	0.4367	M(PK) 1	0.3103	0.3103	0.3103	0.3103	0.3103		
M(PK) 1	0.3103	0.3103	0.3103	0.3103	0.3103	M(PK) 2	0.3175	0.3175	0.3175	0.3200	0.2762	TURN(PRI)	33.599	33.599	33.599	31.833	30.882		
TURN(PRI)	33.599	33.599	33.599	33.599	33.599	UUBAR	0.001	-0.0090	-0.0311	-0.0311	-0.0311	UUBAR	0.4230	0.4529	0.4715	0.5227	0.6186		
UUBAR	0.4230	0.4529	0.4715	0.5227	0.6186	EFP	1.0109	1.0205	1.0205	1.0205	1.0205	EFP	1.0109	1.0205	1.0205	1.0205	1.0205		
EFP	1.0109	1.0205	1.0205	1.0205	1.0205	EFF	1.0111	1.0205	1.0205	1.0205	1.0205	EFF	1.0111	1.0205	1.0205	1.0205	1.0205		
EFF	1.0111	1.0205	1.0205	1.0205	1.0205	INCID	5.311	5.311	5.311	5.311	5.311	INCID	5.311	5.311	5.311	5.311	5.311		
INCID	5.311	5.311	5.311	5.311	5.311	DEV	8.330	6.945	7.562	7.233	9.081	UUBAR	0.1899	0.1566	0.1244	0.1862	0.1862		
UUBAR	0.1862	0.1566	0.1244	0.1862	0.1862	STATION 2 - STATION 2A	0.3114	0.3093	0.3083	0.3076	0.3069	STATION 2 - STATION 2A	0.3114	0.3093	0.3083	0.3076	0.3069		
STATION 2 - STATION 2A	0.3114	0.3093	0.3083	0.3076	0.3069	DFAC	0.7160	0.6064	0.5808	0.5215	0.5739	EFFP	0.5682	0.5682	0.5682	0.5682	0.5682		
EFFP	0.5682	0.5682	0.5682	0.5682	0.5682	INCID	-3.33	-2.00	-1.89	-1.01	1.83	INCID	-3.33	-2.00	-1.89	-1.01	1.83		
INCID	-3.33	-2.00	-1.89	-1.01	1.83	LOSS PARA	1.0621	0.7635	0.6699	0.0891	0.0891	LOSS PARA	1.0621	0.7635	0.6699	0.0891	0.0891		
LOSS PARA	1.0621	0.7635	0.6699	0.0891	0.0891	DEV	2.80	20.54	24.05	24.05	24.05	DEV	2.80	20.54	24.05	24.05	24.05		
DEV	2.80	20.54	24.05	24.05	24.05	DIA	33.564	34.992	36.420	37.276	39.276	DIA	33.564	34.992	36.420	37.276	39.276		

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 89.81

CORRECTED WEIGHT FLOW = 76.68

CORRECTED ROTOR SPEED = 3457.51

INLET GUIDE VANE

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	38.900	37.200	BETA 2	53.273	53.632	53.871	55.309	55.871
V 0	324.26	324.26	324.26	324.26	324.26	BETA(PRI) 1	31.419	33.268	36.301	39.494	44.419
V 1	473.03	471.85	464.56	457.66	433.83	BETA(PRI) 2	0.829	2.704	7.503	11.909	18.032
VZ 0	324.26	324.26	324.26	324.26	324.26	V 1	473.03	471.85	464.56	457.66	433.83
VZ 1	388.43	377.83	368.07	364.54	346.93	V 2	631.65	637.59	624.15	615.45	591.48
V-THETA 0	0.000	0.000	0.000	0.000	0.000	VZ 1	388.43	377.83	368.07	364.54	346.93
V-THETA 1	269.96	282.65	283.45	276.70	260.48	VZ 2	384.46	381.28	370.10	362.87	336.64
M 0	0.2929	0.2929	0.2929	0.2929	0.2929	V-THETA 1	269.96	282.65	283.45	276.70	260.48
M 1	0.4316	0.4305	0.4236	0.4171	0.3946	V-THETA 2	501.17	511.02	502.58	497.09	486.33
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	455.2	451.9	456.7	472.4	485.7
UBAR	0.0153	-0.0176	0.0171	0.0259	0.0194	V(PRI) 2	384.5	381.7	373.3	370.9	354.0
DFAC	-0.057	-0.008	0.017	0.032	0.015	VTHETA PRI	-237.3	-247.9	-270.4	-300.4	-340.0
EFP	0.9970	1.0254	1.0042	0.9867	0.8233	VTHETA PR2	-5.6	-18.0	-48.7	-76.5	-109.6
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	507.23	530.54	533.84	577.14	600.44
DEV	7.300	6.100	6.100	7.700	8.400	U 2	506.73	529.03	551.33	573.62	595.92
						H 1	0.4316	0.4305	0.4236	0.4171	0.3946
						H 2	0.5723	0.5784	0.5652	0.5322	0.4967
						M(PRI) 1	0.4153	0.4122	0.4164	0.4305	0.4419
						M(PRI) 2	0.3484	0.3463	0.3381	0.3352	0.3185
						TURN(PRI)	30.590	30.564	28.798	27.585	26.387
						UUBAR	0.0639	-0.0039	-0.0086	0.0145	0.0739
						DFAC	0.2578	0.3675	0.3944	0.4310	0.4967
						EFFP	0.8534	0.9688	0.9546	0.9314	0.8628
						EFF	0.8509	0.9682	0.9538	0.9362	0.8600
						INCID	-0.02	-2.37	-2.93	-2.93	-0.94

STATION 2 - STATION 2A

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
BETA 2	52.507	53.273	53.632	53.871	55.309	BETA 2	53.871	52.922	51.922	50.922	49.922
BETA 3	25.315	21.070	17.331	21.922	26.341	BETA 3	615.45	591.48	534.27	434.27	434.27
V 2	631.65	631.59	624.15	615.45	606.34	V 2	381.28	362.87	336.64	318.00	298.00
V 2A	369.95	43.62	463.26	466.34	434.27	V 2A	402.77	442.23	432.62	389.18	350.17
VZ 2	334.43	402.77	51.02	502.58	497.09	VZ 2	158.19	155.17	138.00	174.11	192.69
V-THETA 2	501.17	51.02	51.02	51.02	51.02	V-THETA 2	0.5784	0.5652	0.5563	0.5322	0.5108
V-THETA 2A	158.19	155.17	138.00	174.11	192.69	V-THETA 2A	2.17.71	1.7.97	2.2.56	2.6.98	3.9.27
M 2	0.5723	0.5723	0.5723	0.5723	0.5723	M 2	0.3854	0.4141	0.4167	0.3867	0.3185
M 2A	0.3284	0.3284	0.3284	0.3284	0.3284	M 2A	2.19.2	32.20.3	36.30.1	31.94.9	28.96.8
TURN	2.19.2	32.20.3	0.1923	0.1154	0.1205	TURN	0.2659	0.2659	0.1702	0.1702	0.1702
UUBAR	0.2659	0.2659	0.2659	0.2659	0.2659	UUBAR	0.1154	0.1205	0.1205	0.1205	0.1205

DFAC	0.6408	0.5665	0.5235	C.4911	0.5108
EFFF	0.6471	0.7631	0.8421	0.8359	0.8226
INCLD	-5.19	-4.43	-4.07	-3.83	-2.39
LOSS PARA	1.0033	.07853	.05012	.05273	.07435
DEV	25.96	21.71	17.97	22.56	26.98
DIA	33.564	34.992	36.420	37.848	39.276

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 89.76

CORRECTED WEIGHT FLOW = 83.42

CORRECTED ROTIK SPEED = 3455:95

INLET GUIDE VANE		STATION 0 - STATION 1										STATION 1 - STATION 2										
		PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10			
DIA	33.622	35.167	36.711	38.256	39.801	39.801	39.801	DIA	33.589	35.067	36.545	38.023	39.501	BETA 0	0.000	0.000	0.000	0.000	0.000			
BETA 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	36.800	37.600	37.200	BETA 1	0.000	0.000	0.000	0.000	0.000			
BETA 1	34.800	36.800	37.600	37.200	36.900	36.900	36.900	BETA 2	49.556	49.511	50.020	50.255	50.255	BETA 2	0.000	0.000	0.000	0.000	0.000			
V 0	355.88	355.88	355.88	355.88	355.88	355.88	355.88	BETA(PR) 1	24.977	26.238	27.606	29.506	33.309	V 0	0.000	0.000	0.000	0.000	0.000			
V 1	533.66	533.66	522.99	511.42	480.18	480.18	480.18	BETA(PR) 2	1.002	2.635	7.119	11.660	16.996	V 1	0.000	0.000	0.000	0.000	0.000			
VZ 0	355.87	355.87	355.87	355.87	355.87	355.87	355.87	V 1	538.94	533.66	522.99	511.42	480.18	VZ 0	0.000	0.000	0.000	0.000	0.000			
VZ 1	427.32	414.36	407.36	383.99	383.99	383.99	383.99	V 2	655.76	666.30	650.99	638.70	617.69	VZ 1	0.000	0.000	0.000	0.000	0.000			
V-THETA 0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	VZ 1	442.55	427.32	414.36	407.36	383.99	V-THETA 0	0.000	0.000	0.000	0.000	0.000			
V-THETA 1	319.68	319.10	309.20	288.31	288.31	288.31	288.31	VZ 2	425.40	429.97	418.28	411.54	394.94	V-THETA 1	0.3221	0.3221	0.3221	0.3221	0.3221			
M 0	0.3221	0.3221	0.3221	0.3221	0.3221	0.3221	0.3221	V-THETA 2	307.58	319.58	319.10	309.20	288.31	M 0	0.4383	0.4383	0.4383	0.4383	0.4383			
M 1	0.4945	0.4894	0.4791	0.4683	0.4580	0.4480	0.4383	V(PR) 1	485.4	476.4	476.1	487.4	494.7	TURN	-34.80	-37.60	-37.20	-36.90	-36.80			
UUBAR	0.0137	-0.0157	0.0039	0.0285	0.2110	0.2110	0.2110	V(PR) 2	425.5	430.4	421.5	420.2	413.0	UUBAR	0.0000	0.0000	0.0000	0.0000	0.0000			
DFAC	-0.0349	-0.0058	0.014	0.077	0.194	0.194	0.194	VTHETA PRI	-199.4	-210.6	-234.5	-267.7	-311.0	EFFF	0.8106	0.8106	0.8106	0.8106	0.8106			
EFFF	0.9971	1.0194	1.0047	0.9838	0.9838	0.9838	0.9838	VTHETA PK2	-7.4	-19.8	-52.2	-84.9	-120.7	INCID	27.3001	27.7001	28.1001	28.1001	28.1001			
INCID	*****	26.9001	27.3001	27.7001	28.1001	28.1001	28.1001	U 1	507.00	530.30	553.59	576.88	600.74	U 1	0.0000	0.0000	0.0000	0.0000	0.0000			
DEV	7.300	6.100	6.100	7.700	8.400	8.400	8.400	M 1	0.4945	0.4894	0.4844	0.4791	0.4481	M 1	0.5983	0.6033	0.5942	0.5819	0.5604			
SLOTTED STATOR 3											M 2	0.5983	0.6033	0.5942	0.5819	0.5604	M 2	0.5983	0.6033	0.5942	0.5819	0.5604
STATION 2 - STATION 2A											M(PK) 1	0.4454	0.4369	0.4362	0.4461	0.4516	M(PK) 1	0.3882	0.3936	0.3848	0.3749	0.3749
STATION 2 - STATION 2A											TURN(PR)	23.255	23.603	22.386	21.649	22.087	TURN(PR)	0.0000	0.0000	0.0000	0.0000	0.0000
STATION 2 - STATION 2A											UUBAR	-0.0666	-0.0252	-0.0214	-0.0214	-0.0345	UUBAR	0.0000	0.0000	0.0000	0.0000	0.0000
STATION 2 - STATION 2A											UFAC	0.2809	0.2636	0.2817	0.3030	0.3492	UFAC	0.88685	1.0747	1.0496	1.0285	0.9586
STATION 2 - STATION 2A											EFFP	0.8666	1.0759	1.0504	1.0590	0.9579	EFFP	0.4454	0.4369	0.4362	0.4461	0.4516
STATION 2 - STATION 2A											INCID	-7.18	-9.40	-9.72	-9.72	-6.28	INCID	0.0000	0.0000	0.0000	0.0000	0.0000
STATION 2 - STATION 2A											DEV	6.382	4.595	4.959	5.040	6.126	DEV	0.0000	0.0000	0.0000	0.0000	0.0000

	D <small>DFAC</small>	E <small>FPP</small>	I <small>NICID</small>	O <small>NS PARA</small>	P <small>DEV</small>
0.5135	0.4932	0.4260	0.3798	0.4180	
0.6459	0.7137	0.8519	0.7747	0.5558	
-8.14	-7.89	-7.68	-7.82	-7.44	
0.9355	0.8571	0.4500	0.0275	-0.0910	
25.89	18.64	17.96	23.53	29.68	
1.00	1.00	1.00	1.00	1.00	
					16.27

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.00

CORRECTED WEIGHT FLOW = 68.98

CORRECTED ROTOR SPEED = 3849.81

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1						STATION 1 - STATION 2					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.200	37.200	36.900
BETA 1	3.800	36.800	37.600	37.200	36.900	BETA 2	56.370	56.906	60.289	67.736	67.736
V 0	289.21	289.21	289.21	289.21	289.21	BETA(PRI) 1	44.023	45.937	48.764	51.429	55.359
V 1	413.97	414.14	414.14	407.31	400.78	BETA(PRI) 2	3.006	6.900	10.892	16.820	22.354
VZ 0	289.21	289.21	289.21	289.21	289.21	V 1	413.97	414.14	407.31	400.78	380.33
VZ 1	339.93	331.62	322.71	319.24	304.15	V 2	654.77	651.71	663.48	627.19	613.67
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	339.93	331.62	322.71	319.24	304.15
V-THETA 1	236.26	248.08	248.52	242.31	228.36	VZ 2	362.63	355.84	334.97	310.85	232.51
M 0	0.2608	0.2608	0.2608	0.2608	0.2608	V-THETA 1	236.26	248.08	242.31	228.36	228.36
M 1	0.3761	0.3762	0.3762	0.3638	0.3447	V-THETA 2	54.19	545.99	549.42	544.74	567.92
TURN	-34.80	-36.80	-37.20	-37.20	-36.90	V(PRI) 1	472.7	476.8	489.6	512.0	535.1
UUBAR	0.0412	-0.0044	0.0236	0.0457	0.2018	V(PRI) 2	363.1	358.4	341.1	324.7	251.4
DFAC	-0.044	0.008	0.034	0.050	0.100	V(THETA PR1	-328.5	-342.7	-368.2	-400.3	-440.2
EFFF	0.9764	1.0176	0.9915	0.9690	0.8037	V(THETA PR2	-19.0	-43.1	-64.5	-94.0	-95.6
INCID	*****	26.9001	27.3001	27.001	28.1001	U 1	568.79	590.73	616.68	642.62	668.57
DEV	7.300	6.100	6.100	7.700	8.400	U 2	566.23	589.05	613.88	638.71	663.54
						M 1	0.3761	0.3762	0.3638	0.3447	0.3447
						M 2	0.8897	0.5878	0.5790	0.5620	0.5463
						M(PRI) 1	0.4294	0.4332	0.4445	0.4647	0.4850
						M(PRI) 2	0.3270	0.3233	0.3070	0.2910	0.2238
						TURN(PRI)	41.017	39.037	37.872	34.509	33.005
						UUBAR	0.0819	0.0553	0.1062	0.1842	0.3644
						DFAC	0.924	0.5104	0.5739	0.6384	0.8360
						EFFF	0.9115	0.9965	0.9675	0.8786	0.7729
						EFF	0.9092	0.9964	0.9666	0.8753	0.7667
						INC ID	12.58	10.30	9.53	9.01	10.00
V 2	654.77	651.71	643.48	627.19	613.67	DEV	8.386	8.860	8.732	10.200	11.484
V2A	298.24	401.24	416.39	437.89	396.49						
VZ 2	362.63	355.84	334.97	310.85	232.51						
VZ 2A	263.98	359.16	383.09	394.23	368.47						
V-THETA 2	545.19	545.99	549.42	546.74	567.92						
V-THETA 2A	129.97	178.87	163.16	190.60	146.41						
M 2	0.5897	0.5878	0.5790	0.5620	0.5463						
M 2A	0.2574	0.3537	0.3671	0.3864	0.3486						
TURN	30.157	30.431	35.561	34.486	46.066						
UUBAR	0.3399	0.1853	0.1617	0.0924	0.1743						
DFAC	0.4152	0.6300	0.6261	0.5696	0.6923						
EFFF	0.5697	0.6744	0.7030	0.8617	0.9935						
INC ID	-1.33	-0.79	0.93	2.59	10.04						
LOSS PARA	.12793	.07260	.06771	.03923	.07897						
DEV	26.85	27.12	23.71	26.44	22.31						
OIA	33.564	34.932	36.420	37.848	39.276						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.54

CORRECTED WEIGHT FLOW = 72.87

CORRECTED ROTOR SPEED = 3870.98

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	38.200	39.800	BETA 2	55.999	56.578	57.377	58.439	62.824
V 0	306.79	306.79	306.79	306.79	306.79	BETA(PR) 1	40.373	42.342	45.287	48.152	52.521
V 1	447.55	447.04	439.63	432.51	409.07	BETA(PR) 2	3.351	6.475	10.449	16.464	22.088
VZ 0	306.79	306.79	306.79	306.79	306.79	V 1	447.55	447.04	439.63	432.51	409.07
VZ 1	367.50	357.96	348.32	344.51	327.13	V 2	658.33	660.20	655.50	631.90	620.66
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	367.50	357.96	348.32	344.51	327.13
V-THETA 1	255.42	267.79	268.24	261.50	245.61	VZ 2	368.14	363.64	353.39	333.88	283.47
M 0	0.2769	0.2769	0.2769	0.2769	0.2769	V-THETA 1	255.42	267.79	268.24	261.50	245.61
M 1	0.4075	0.4071	0.4001	0.3934	0.3715	V-THETA 2	545.78	551.02	552.08	541.55	521.15
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	482.4	484.3	495.1	516.4	537.6
UBAR	0.0485	0.0066	0.0315	0.0525	0.2243	V(PR) 2	368.8	366.0	359.3	348.2	305.9
DFAC	-0.057	-0.009	0.017	0.033	0.088	V(THETA PR1	-312.5	-326.2	-351.8	-384.7	-426.6
EFFP	0.9710	1.0055	0.9837	0.9635	0.7947	V(THETA PR2	-21.6	-41.3	-65.2	-98.7	-115.0
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	567.89	593.98	620.07	646.16	672.25
DEV	7.300	6.100	6.100	7.700	8.400	U 2	567.33	592.29	617.26	642.22	667.18
						H 1	0.4075	0.4071	0.4001	0.3934	0.3715
						H 2	0.5936	0.5964	0.5915	0.5737	0.5542
						H(PR) 1	0.4393	0.4410	0.4506	0.4697	0.4882
						H(PR) 2	0.3325	0.3306	0.3243	0.3131	0.2732
						TURN(PR)	37.022	35.867	34.838	31.688	30.432
						UDBAR	0.0510	-0.0008	0.0026	0.0643	0.1901
						DFAC	0.4755	0.4897	0.5268	0.5782	0.7064
						EFFP	0.9016	1.0129	1.0367	0.9749	0.8464
						EFF	0.8991	1.0132	1.0377	0.7742	0.8420
						INCID	8.93	6.70	6.06	5.73	7.16

STATION 2 - STATION 2A

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
BETA 2	55.999	56.578	57.377	58.439	62.824	TURN(PR)	37.022	35.867	34.838	31.688	30.432
BETA 3	25.978	26.634	21.897	26.122	24.081	UDBAR	0.0510	-0.0008	0.0026	0.0643	0.1901

V 2	658.33	660.20	655.50	637.90	620.66	DEV	8.731	8.435	8.289	9.844	11.218
VZ 2A	325.34	413.92	431.84	451.69	420.44						
VZ 2A	368.14	363.64	353.39	333.88	283.47						
V-THETA 2	292.47	376.25	400.69	405.55	383.85						
V-THETA 2A	545.78	551.02	552.08	543.55	552.15						
M 2	142.51	172.53	161.05	198.87	171.55						
M 2A	0.5936	0.5964	0.5915	0.5737	0.5542						
TURN	30.021	31.944	35.440	32.317	38.743						
UDBAR	0.2926	0.1843	0.1747	0.1170	0.1750						
DFAC	0.7614	0.6231	0.6126	0.5482	0.6249						
EFFP	0.5960	0.6422	0.6674	0.7607	0.9026						
INCID	-1.170	-1.12	-0.32	0.74	5.12						
LOSS PARA	-11.041	0.07329	0.07319	0.0955	0.0784						
DEV	26.62	25.27	22.54	26.76	24.72						
DIA	33.564	34.992	36.420	37.848	39.276						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.28

CORRECTED WEIGHT FLOW = 75.89

CORRECTED ROTOR SPEED = 3860.80

INLET GUIDE VANE

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	38.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	55.393	56.097	56.952	57.353	60.533
V 0	320.61	320.61	320.61	320.61	320.61	BETA(PR) 1	38.287	40.138	43.043	45.055	50.337
V 1	464.67	464.93	458.08	452.17	428.45	BETA(PR) 2	2.940	5.341	9.495	14.641	20.487
V 2	320.61	320.61	320.61	320.61	320.61	V 1	464.07	464.93	458.08	452.17	428.45
VZ 0	381.57	372.29	362.93	360.17	342.62	V 2	663.95	669.67	662.39	651.65	631.08
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	381.57	372.29	362.93	360.17	342.62
V-THETA 1	265.19	278.51	279.49	273.38	257.25	VZ 2	377.09	373.53	361.23	351.54	310.44
M 0	0.2896	0.2896	0.2896	0.2896	0.2896	V-THETA 1	265.19	278.51	279.49	273.38	257.25
M 1	0.4239	0.4239	0.4175	0.4119	0.3896	V-THETA 2	544.47	555.81	555.22	548.69	549.44
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	486.1	487.0	496.6	517.1	536.8
UUBAR	-0.0566	-0.0132	0.0361	0.2214	0.2214	V(PRI) 2	377.6	375.52	366.2	363.3	331.4
DFAC	-0.050	-0.004	0.020	0.033	0.086	VTHETA PR1	-301.2	-313.9	-338.9	-371.1	-413.2
EFFP	0.9630	0.5989	0.9785	0.9644	0.7980	VTHETA PR2	-19.4	-34.9	-60.4	-91.8	-116.0
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	566.40	592.42	618.44	644.46	670.48
DEVI	7.300	6.100	6.100	7.700	8.400	U 2	565.84	590.74	615.63	640.53	665.43
						M 1	0.4237	0.4239	0.4175	0.4119	0.3896
						M 2	0.5959	0.6065	0.5989	0.5880	0.5652
						(M(PRI) 1	0.4432	0.4440	0.4525	0.4711	0.4881
						(M(PRI) 2	0.3912	0.3398	0.3312	0.3278	0.2968
						TURN(PRI)	35.348	34.797	33.548	31.213	29.850
						UUBAR	0.0445	-0.0064	-0.0025	0.0288	0.1312
						DFAC	0.4540	0.4686	0.5072	0.5435	0.6458
						EFFP	0.9139	1.0547	1.0572	1.0370	0.8878
						EFF	0.9118	1.0561	1.0588	1.0380	0.8847
						INCID	6.85	4.50	3.81	3.43	4.98
V 2	663.95	669.67	662.39	651.65	631.08						
V 2A	335.14	424.18	452.24	470.83	439.67	DEV	8.320	7.301	7.335	8.021	9.617
VZ 2	377.09	373.53	361.23	351.54	310.44						
VZ 2A	300.94	386.60	420.29	424.07	398.54						
V-THETA 2	546.47	555.81	555.22	548.69	549.44						
V-THETA 2A	147.48	174.56	166.96	204.57	185.68						
M 2	0.5999	0.6065	0.5989	0.5880	0.5652						
M 2A	0.2944	0.3755	0.4009	0.4174	0.3887						
TURN	29.285	31.796	35.786	31.601	35.553						
UUBAR	0.2971	0.1976	0.1601	0.1290	0.1789						
DFAC	0.7459	0.6149	0.5840	0.5280	0.5875						
EFFP	0.5927	0.6638	0.6955	0.7031	0.8412						
INCID	-2.31	-1.60	-0.75	-0.35	2.83						
LOSS PARA	.11194	.07577	.06772	.09453	.07908						
DEV	26.75	24.94	22.31	26.39	25.62						
DIA	33.564	34.992	36.420	37.848	39.276						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.05

INITIATE VANE

	DFAC	EFFP	INCID	LOSS PARA	DEV	DEV
0.6779	0.5890	0.5628	0.5140	0.5388		
0.6612	0.6899	0.7311	0.6946	0.7851		
-3.67	-2.64	-2.05	-1.90	0.23		
.1005	.0716	.01392	-0.0669	.07392		
27.84	23.74	20.24	24.64	27.44		
23.65	26.62	27.62	26.66	26.72		

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.14

CORRECTED WEIGHT FLOW = 84.71

CORRECTED ROTOR SPEED = 3855.26

INLET GUIDE VANE		STATION 0 - STATION 1					STATION 1 - STATION 2					FLOW GENERATION ROTOR					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501						
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.200	37.200	36.900						
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	52.820	53.118	53.240	53.240	54.940						
V 0	362.04	362.04	362.04	362.04	362.04	BETA(PR) 1	31.054	32.728	35.638	38.832	43.760						
V 1	530.98	531.20	524.17	516.58	490.05	BETA(PR) 2	0.932	3.132	7.433	11.923	17.362						
VZ 0	362.04	362.04	362.04	362.04	362.04	V 1	530.98	531.20	524.17	516.58	490.05						
VZ 1	436.02	425.35	415.29	411.47	391.88	V 2	706.72	710.83	700.03	689.60	665.71						
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	436.02	425.35	415.29	411.47	391.88						
V-THETA 1	303.04	318.20	319.82	312.33	294.23	VZ 2	433.74	429.52	420.14	412.70	382.40						
M 0	0.3278	0.3278	0.3278	0.3278	0.3278	V-THETA 1	303.04	318.20	319.82	312.33	294.23						
M 1	0.4868	0.4870	0.4803	0.4730	0.4477	V-THETA 2	557.97	566.38	559.94	552.47	544.91						
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PRI) 1	509.0	505.6	511.0	528.2	542.6						
UBAR	0.0484	0.0085	0.0304	0.0560	0.2335	V(PRI) 2	433.8	430.2	423.7	421.8	400.7						
DFAC	-0.062	-0.016	0.021	0.074	0.074	VTHETA PR1	-262.5	-273.4	-297.7	-331.2	-375.3						
EFFP	0.9693	1.0007	0.9825	0.9526	0.7976	VTHETA PR2	-7.1	-23.5	-54.8	-87.1	-119.6						
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	565.59	591.57	617.55	643.53	669.52						
DEV	7.300	6.100	6.100	7.700	8.400	U 2	565.03	589.89	614.75	639.61	664.46						
SLOTTED STATOR 3		M 1	0.4868	0.4870	0.4730	M 2	511.0	505.6	509.0	528.2	542.6						
STATION 2 - STATION 2A		(MPRI) 1	0.4660	0.4640	0.4640	(MPRI) 2	433.8	430.2	423.7	421.8	400.7						
PCT. SPAN	90	70	50	30	10	TURN(PR)	30.122	29.586	28.204	26.909	26.398						
BETA 2	52.160	52.825	53.118	53.240	54.940	UUBAR	0.0826	0.0165	0.0100	0.0195	0.0844						
BETA 3	25.917	21.297	17.658	23.018	27.004	DFAC	0.3475	0.3553	0.3783	0.4121	0.4857						
						EFFP	0.9168	1.0371	1.0371	1.0141	1.0054						
						EFF	0.9168	1.0380	1.0141	1.0141	1.0054						
						INC1D	-0.39	-2.91	-3.59	-3.59	-1.60						
V 2	706.72	710.83	700.03	689.60	665.71	DEV	6.312	5.092	5.273	5.303	6.492						
V 2A	412.98	496.19	529.12	536.93	489.18												
VZ 2	433.74	429.52	420.14	412.70	382.40												
VZ 2A	371.45	462.31	504.19	494.18	455.85												
V-THETA 2	557.97	566.38	559.94	552.47	544.91												
V-THETA 2A	180.50	180.22	160.50	209.95	222.12												
M 2	0.6440	0.6486	0.6313	0.6265	0.6016												
M 2A	0.3663	0.4442	0.4740	0.4807	0.4357												
TURN	26.223	31.528	35.460	30.222	27.936												
UUBAR	0.2992	0.1879	0.1236	0.1154	0.2035												
DFAC	0.6385	0.5389	0.5038	0.4570	0.5045												
EFFP	0.5876	0.7473	0.7933	0.7720	0.6810												
INC1D	-5.56	-4.87	-4.58	-4.46	-2.76												
LOSS PARA	.11286	.07658	.05330	.05010	.08836												
DEV	26.56	21.94	18.30	23.66	27.64												
DIA	33.564	34.992	36.420	37.848	39.276												

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 100.32

CORRECTED WEIGHT FLOW = 90.04

CORRECTED ROTOR SPEED = 3862.14

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1

PCT SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	49.859	50.100	50.498	50.169	50.487
V 0	387.96	387.96	387.96	387.96	387.96	BETA(PR) 1	25.878	27.707	30.780	34.337	39.730
V 1	584.70	581.27	571.73	561.23	530.19	BETA(PR) 2	1.394	2.966	7.109	11.968	17.259
VZ 0	387.96	387.96	387.96	387.96	387.96	V 1	584.70	581.27	571.73	561.23	530.19
VZ 1	480.12	452.98	447.03	423.98	V 2	VZ 1	725.55	723.73	723.73	729.03	685.87
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 2	480.12	463.44	452.98	447.03	423.98
V-THETA 1	333.69	348.19	348.84	339.32	318.33	VZ 2	467.74	473.59	460.37	454.15	434.54
M 0	0.3518	0.3518	0.3518	0.3518	0.3518	-V-THETA 1	333.69	344.19	348.84	359.32	318.33
M 1	0.5388	0.5354	0.5262	0.5160	0.4860	-V-THETA 2	554.65	566.40	558.43	544.49	530.66
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	533.6	525.7	527.2	541.4	551.3
UUBAR	0.0448	0.0141	0.0332	0.0589	0.2415	V(PR) 2	474.2	463.9	464.2	455.0	455.0
DFAC	-0.092	-0.038	-0.011	0.008	0.005	VTHETA PR1	-232.9	-244.4	-269.8	-305.4	-352.4
EFFP	0.9740	0.9957	0.9806	0.9587	0.7987	VTHETA PR2	-11.4	-24.5	-57.4	-96.3	-135.0
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	566.59	592.62	618.65	644.68	670.71
DEV	7.300	6.100	6.100	7.700	8.400	M 1	566.03	590.94	615.85	640.75	665.66
						M 2	0.5388	0.5354	0.5262	0.5160	0.4860
						M(PR) 1	0.6650	0.6339	0.6488	0.6260	
						M(PR) 2	0.4917	0.4843	0.4852	0.4977	0.5054
						TURN(PR)	0.4288	0.4559	0.4256	0.4248	0.4153
						UBAR	24.484	24.741	23.671	22.369	22.472
						DFAC	0.1168	0.1152	0.0161	0.0298	0.0550
						EFFP	0.2884	0.2724	0.2959	0.3187	0.3623
						FFF	0.8789	1.1043	1.0892	1.0595	1.1153
						INCID	0.8768	1.1064	1.0910	1.1178	1.1178
							-5.56	-7.93	-8.45	-8.08	-5.63

STATION 2 - STATION 2A

V 2	725.55	738.30	723.73	709.03	685.87	DEV	6.774	4.926	4.949	5.348	6.389
VZ 2A	507.80	558.45	515.73	598.60	531.43						
VZ 2	467.74	473.59	460.37	454.15	434.54						
VZ 2A	458.70	527.73	548.17	551.86	464.77						
V-THETA 2	554.65	566.40	558.43	544.49	530.66						
M 2	217.84	182.66	175.99	231.89	257.70						
M 2A	0.6650	0.6787	0.6639	0.6488	0.6260						
M 4569	0.4569	0.5094	0.5344	0.5435	0.4805						
TURN	24.455	31.008	32.699	27.377	21.680						
UBAR	0.2410	0.1900	0.1211	0.0884	0.2329						
DFAC	0.4938	0.4703	0.4450	0.3650	0.4219						
EFFP	0.6962	1.4601	-0.8497	1.0826	0.7747						
INCID	-7.84	-7.60	-7.20	-7.53	-7.01						
LOSS PARA	.09131	.07858	.05248	.03846	.00736						
DEV	26.04	19.73	18.44	20.43	29.65						
DIA	33.564	34.992	36.420	37.848	39.426						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 110.01

CORRECTED WEIGHT FLOW = 75.90

CORRECTED ROTOR SPEED = 4235.53

INLET GUIDE VANE

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT SPAN
DIA	33.622	35.167	36.711	38.256	39.801	DIA
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2
V 0	32.0.66	320.66	320.66	320.66	320.66	BETA(PR) 1
V 1	446.11	465.07	457.05	450.31	424.82	BETA(PR) 2
VZ 0	322.66	322.66	322.66	322.66	322.66	V 1
VZ 1	362.75	372.39	362.11	355.69	339.72	V 2
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1
V-THETA 1	266.02	278.58	278.86	272.26	255.07	VZ 2
M 0	0.2896	0.2896	0.2896	0.2896	0.2896	V-THETA 1
M 1	0.4250	0.4240	0.4165	0.4101	0.3862	V-THETA 2
TURN	-34.80	-36.10	-37.60	-37.20	-36.90	V(PRI) 1
UUBAR	0.0060	-0.0289	0.0024	0.0205	0.0233	V(PRI) 2
DFAC	-0.053	-0.005	0.022	0.037	0.094	V(THETA PR1)
EFFP	1.0050	1.0362	1.0088	0.9918	0.8062	V(THETA PR2)
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1
DEV	7.300	6.100	6.100	7.700	8.400	U 2

SLOTTED STATOR 3

PCT. SPAN	90	70	50	30	10	PCT SPAN
BETA 2	56.043	56.679	58.229	59.974	67.494	M(PR) 1
BETA 3	27.139	26.600	22.522	24.966	19.043	M(PR) 2
V 2	716.32	719.67	701.46	689.52	676.04	TURN(PR)
V 2A	328.41	452.12	464.48	488.23	432.94	UUBAR
VZ 2	400.11	395.33	372.50	345.03	258.78	DFAC
VZ 2A	292.25	404.26	429.06	442.61	409.24	EFFP
V-THETA 2	594.15	601.36	601.46	596.98	624.56	EFF
V-THETA 2A	149.80	202.44	177.91	206.07	141.26	INCID
M 2	0.4464	0.6504	0.6383	0.6192	0.6015	DEV
M 2A	0.2858	0.3974	0.4084	0.4228	0.3791	
TURN	28.204	30.079	35.707	35.008	48.451	
UUBAR	0.3476	0.1933	0.1697	0.0975	0.2013	

DFAC	0.8003	0.6136	0.6159	0.5607	0.7117
EFFP	0.5309	0.6502	0.6549	0.7836	0.8967
INCID	-1.66	-1.02	0.53	2.27	9.79
LOSS PARA	1.2979	0.07561	0.07132	0.04171	0.0275
DEV	21.78	27.24	23.16	25.61	19.68
DIA	33.564	34.992	36.420	37.848	39.276

STATION 0 - STATION 1

PCT. SPAN	90	70	50	30	10	PCT SPAN
DIA	33.564	34.992	36.420	37.848	39.276	STATION 1 - STATION 2
BETA 0	0.000	0.000	0.000	0.000	0.000	33.589
BETA 1	34.800	36.800	37.600	37.200	36.900	34.800
V 0	32.0.66	320.66	320.66	320.66	320.66	36.679
V 1	446.11	465.07	457.05	450.31	424.82	42.075
VZ 0	322.66	322.66	322.66	322.66	322.66	58.229
VZ 1	362.75	372.39	362.11	355.69	339.72	44.918
V-THETA 0	0.00	0.00	0.00	0.00	0.00	42.173
V-THETA 1	266.02	278.58	278.86	272.26	255.07	27.886
M 0	0.2896	0.2896	0.2896	0.2896	0.2896	27.886
M 1	0.4240	0.4240	0.4165	0.4101	0.3862	27.886
TURN	-34.80	-36.10	-37.60	-37.20	-36.90	59.698
UUBAR	0.0060	-0.0289	0.0024	0.0205	0.0233	59.698
DFAC	-0.053	-0.005	0.022	0.037	0.094	59.698
EFFP	1.0050	1.0362	1.0088	0.9918	0.8062	59.698
INCID	*****	26.9001	27.3001	27.7001	28.1001	59.698
DEV	7.300	6.100	6.100	7.700	8.400	59.698

STATION 1 - STATION 2

PCT. SPAN	90	70	50	30	10	PCT SPAN
DIA	33.564	34.992	36.420	37.848	39.276	STATION 1 - STATION 2
BETA 0	0.000	0.000	0.000	0.000	0.000	33.589
BETA 1	34.800	36.800	37.600	37.200	36.900	34.800
V 0	32.0.66	320.66	320.66	320.66	320.66	36.679
V 1	446.11	465.07	457.05	450.31	424.82	42.075
VZ 0	322.66	322.66	322.66	322.66	322.66	58.229
VZ 1	362.75	372.39	362.11	355.69	339.72	44.918
V-THETA 0	0.00	0.00	0.00	0.00	0.00	42.173
V-THETA 1	266.02	278.58	278.86	272.26	255.07	27.886
M 0	0.2896	0.2896	0.2896	0.2896	0.2896	27.886
M 1	0.4240	0.4240	0.4165	0.4101	0.3862	27.886
TURN	-34.80	-36.10	-37.60	-37.20	-36.90	59.698
UUBAR	0.0060	-0.0289	0.0024	0.0205	0.0233	59.698
DFAC	-0.053	-0.005	0.022	0.037	0.094	59.698
EFFP	1.0050	1.0362	1.0088	0.9918	0.8062	59.698
INCID	*****	26.9001	27.3001	27.7001	28.1001	59.698
DEV	7.300	6.100	6.100	7.700	8.400	59.698

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 110.09

CORRECTED WEIGHT FLOW = 78.46

INLET GUIDE VANE				CORRECTED ROTUR SPEED = 4238.62				FLOW GENERATION ROTOR			
STATION 0 - STATION 1				STATION 1 - STATION 2							
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.59	35.067	36.445	38.023	39.301
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	55.960	56.790	57.686	58.626	63.593
V 0	332.52	332.52	332.52	332.52	332.52	BETA(PR) 1	41.941	43.681	46.193	49.090	53.019
V 1	475.20	476.93	472.77	464.31	442.18	BETA(PR) 2	3.917	6.474	10.548	15.919	21.074
VZ 0	332.51	332.51	332.51	332.51	332.51	V 1	475.0	476.93	477.77	464.31	442.18
VZ 1	350.21	381.89	374.57	369.84	353.61	V 2	716.53	721.55	715.46	701.62	684.65
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	390.21	381.89	374.57	369.84	353.61
V-THETA 1	271.20	285.69	288.46	280.12	265.49	VZ 2	401.09	395.20	382.46	365.28	304.49
M 0	0.3005	0.3005	0.3005	0.3005	0.3005	V-THETA 1	271.20	285.69	288.46	280.12	265.49
M 1	0.4336	0.4336	0.4313	0.4233	0.4025	V-THETA 2	593.70	603.70	599.03	613.21	
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PR) 1	524.6	528.1	541.1	564.7	588.6
UUBAR	0.0101	-0.0235	-0.0022	0.0571	0.2297	V(PR) 2	402.0	397.7	389.0	379.8	326.3
DFAC	-0.035	-0.007	0.025	0.042	0.090	VTHETA PR1	-356.6	-364.7	-390.5	-426.8	-470.6
EFFP	1.0009	1.0318	1.0125	0.9563	0.7877	VTHETA PR2	-27.5	-44.8	-71.2	-104.2	-117.3
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	621.83	650.39	678.96	707.53	736.09
DEV	7.300	6.100	6.100	7.700	8.400	U 2	621.21	648.54	675.88	703.21	730.55
						M 1	0.4336	0.4353	0.4313	0.4233	0.4025
						M 2	0.6468	0.6529	0.6467	0.6320	0.6109
						M(PR) 1	0.4787	0.4819	0.5149	0.358	
						M(PR) 2	0.3629	0.3599	0.3517	0.3421	0.2911
						TURN(PR)	38.024	37.207	35.644	33.171	32.005
						UUBAR	0.0786	0.0293	0.0348	0.0816	0.2208
						DFAC	0.4788	0.4995	0.5385	0.5878	0.7307
						EFFP	0.9078	1.0216	1.0491	1.0055	0.8453
						EFF	0.9050	1.0223	1.0507	1.0057	0.8400
						INCIU	10.50	8.04	6.96	6.67	7.72
						DEV	9.297	8.434	8.388	8.299	10.204
BETA 2	55.960	56.790	57.686	58.626	63.593						
BETA 3	26.769	26.158	22.177	24.652	21.605						
V 2	716.53	721.55	715.46	701.62	684.65						
V 2A	340.38	456.50	478.54	501.37	454.54						
VZ 2	401.09	395.20	382.46	365.28	304.49						
VZ 2A	303.90	409.74	443.13	455.67	422.60						
V-THETA 2	593.75	603.70	604.66	599.03	613.21						
V-THETA 2A	153.30	201.25	180.63	209.12	167.36						
M 2	0.6468	0.6529	0.6467	0.6320	0.6109						
M 2A	0.2969	0.4020	0.4217	0.423	0.3989						
TURN	29.191	30.632	35.509	33.974	41.988						
UUBAR	0.3427	0.2070	0.1868	0.1362	0.2196						
DFAC	0.7814	0.6106	0.6008	0.5489	0.6570						
EFFP	0.5493	0.6462	0.6291	0.7029	0.8015						
INCID	-1.74	-0.91	-0.01	0.93	5.89						
LOSS PARA	.12842	.08131	.07873	.05861	.09950						
DEV	27.41	26.10	22.82	22.29	22.25						
DIA	33.564	34.992	36.420	37.848	39.276						

Table B-2. Blade Element Performance (Continued)

PERCENT OF SIGN SP_{TU} = 110.07

CORRECTED WEIGHT FLOW = 81.00

CORRECTED ROTUR SP_{TED} = 4237.80

INLET GUIDE VANE

FLOW GENERATION ROTOR

STATION 0 - STATION 1						STATION 1 - STATION 2					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	55.650	56.294	57.113	57.715	50.925
V 0	344.41	344.41	344.41	344.41	344.41	BETA(PR) 1	33.004	36.061	40.218	44.494	50.493
V 1	563.11	530.29	509.95	468.68	344.41	BETA(PR) 2	3.632	6.082	10.126	15.108	23.709
VZ 0	344.41	344.41	344.41	344.41	344.41	V 1	563.11	550.10	530.29	509.95	468.68
VZ 1	462.40	440.48	420.15	406.19	374.80	V 2	721.01	727.72	721.41	710.47	693.55
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 1	462.40	440.15	420.15	374.80	374.80
V-THETA 1	321.38	329.52	323.56	308.31	281.40	VZ 2	406.83	403.84	391.71	379.48	337.17
M 0	0.3115	0.3115	0.3115	0.3115	0.3115	V-THETA 1	321.38	329.52	323.56	308.31	281.40
M 1	0.5178	0.5052	0.4862	0.4667	0.4275	V-THETA 2	595.27	605.39	607.79	600.63	538.42
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PK) 1	551.4	544.9	550.2	569.4	589.1
UUBAR	0.0126	0.0366	0.0596	0.2542	0.1266	V(PK) 2	407.6	406.1	397.9	393.1	477.5
DEAAC	-0.184	-0.106	-0.056	-0.015	0.069	V(THETA PR) 1	-300.3	-320.7	-355.3	-399.1	-454.5
EFFP	0.9776	0.9824	0.9626	0.7868	0.7868	V(THETA PR) 2	-25.8	-43.0	-70.0	-102.4	-192.0
INCID	*****	26.9001	27.3001	27.7001	28.1001	U 1	621.71	650.27	678.83	707.39	735.95
DEV	7.300	6.100	6.100	7.700	8.400	U 2	621.09	648.42	675.75	703.08	730.41
SLOTTED STATOR 3											
BETA 2	55.650	56.294	57.113	57.715	50.925	M(PR) 1	0.5070	0.5004	0.5044	0.5211	0.5373
BETA 3	26.532	25.819	21.795	24.558	22.448	M(PR) 2	0.3684	0.3681	0.3600	0.3548	0.4271
V 2	721.01	727.72	721.41	710.47	693.55	TURN(PR)	29.372	29.979	30.092	29.386	26.783
V 2A	348.26	467.21	496.48	516.17	474.92	UJBAR	0.1063	-0.1464	-0.1110	-0.0298	-0.1901
VZ 2	406.83	403.84	391.71	379.48	437.17	DFAC	0.4673	0.4667	0.4662	0.4667	0.4275
VZ 2A	311.58	420.36	460.99	469.48	438.94	EFFP	0.9008	1.0419	1.0454	1.0350	0.8812
V-THETA 2	595.27	605.39	605.79	600.63	538.42	EFF	0.3681	0.4669	1.0469	1.0362	0.8771
V-THETA 2A	155.57	203.92	184.34	214.53	181.35	INCID	1.56	0.42	0.99	2.07	5.13
M 2	0.6517	0.6597	0.6527	0.6414	0.6203	DEV	9.012	8.042	7.966	8.488	12.839
M 2A	0.3042	0.4124	0.4386	0.4563	0.4177	UJBAR	34.992	36.420	37.848	39.276	
TURN	29.118	30.415	35.318	33.157	28.477						
UUBAR	0.3440	0.2084	0.1746	0.1427	0.2188						

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 110%⁴¹

CONNECTED WEIGHTS 25 82

CORRECTED ROTUK SPEED = 4250.91

STATION 0 - STATION 1										STATION 1 - STATION 2									
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10		
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501	BETA 1	34.800	36.800	37.600	37.200	36.900		
BETA 0	0.000	0.000	0.000	0.000	0.000	BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	54.097	55.103	55.608	55.757	59.122		
BETA 1	34.800	36.800	37.600	37.200	36.900	BETA 2	54.097	55.103	55.608	55.757	59.122	BETA(PR)	1	34.807	36.801	37.600	37.200	36.900	
V 0	367.62	367.62	367.62	367.62	367.62	BETA(PR)	1	34.807	36.801	37.600	37.200	36.900	42.910	47.516	49.510	51.510	53.510		
V 1	546.29	544.44	535.76	527.35	500.97	BETA(PR)	2	34.246	4.971	9.050	13.864	16.434	V 1	546.29	544.44	535.96	527.35	500.97	
V2 0	367.62	367.62	367.62	367.62	367.62	V 1	546.29	544.44	535.96	527.35	500.97	V 2	400.62	420.05	440.48	460.91	481.34		
V2 1	448.59	435.95	424.64	420.05	400.62	V 2	738.81	748.53	740.67	730.43	711.79	V 1	0.00	0.00	0.00	0.00	0.00		
V-THETA 0	0.00	0.00	0.00	0.00	0.00	V 1	448.59	435.95	422.64	400.05	388.41	V 2	300.79	318.83	327.01	335.30	345.50		
V-THETA 1	311.77	326.13	327.01	318.83	300.79	V 2	433.25	428.24	418.37	411.01	393.74	V-THETA 1	311.77	326.13	327.01	335.30	345.50		
M 0	0.3329	0.3329	0.3329	0.3329	0.3329	V-THETA 1	311.77	326.13	327.01	335.30	345.50	M 1	0.4998	0.4933	0.4581	0.4130	0.3772		
M 1	0.5015	0.4998	0.4916	0.4833	0.4581	V-THETA 2	598.44	613.93	611.20	603.81	610.91	V(PK) 1	546.3	552.8	557.7	562.5	567.5		
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PK) 1	546.3	552.8	557.7	562.5	567.5	V(PK) 2	0.0229	0.0341	0.0580	0.0916	0.1353		
UUBAR	0.0433	0.0101	0.0341	0.0580	0.1010	V(PK) 2	433.9	429.8	425.6	423.3	423.3	VTHETA PR1	-311.9	-326.1	-333.9	-390.7	-437.4		
DFAC	-0.076	-0.026	-0.000	-0.000	-0.000	VTHETA PR1	-311.9	-326.1	-333.9	-390.7	-437.4	VTHETA PR2	-24.6	-36.5	-66.6	-101.4	-121.8		
EFFP	0.9743	0.9943	0.9797	0.9586	0.8098	VTHETA PR2	623.63	652.28	680.93	709.58	738.23	U 1	27.7001	28.1001	27.7001	27.7001	27.7001		
INC1D	*****	2.6e+001	2.7e+001	2.7e+001	2.7e+001	U 1	623.63	652.28	680.93	709.58	738.23	U 2	623.63	650.43	677.84	705.25	732.67		
DEV	7.300	6.100	6.100	7.700	8.400	M 1	0.5015	0.4998	0.4933	0.4581	0.4130	M 2	0.6764	0.6874	0.6784	0.6676	0.6449		
SLOTTED STATOR 3										SLOTTED STATOR 3									
STATION 2 - STATION 2A										STATION 2 - STATION 2A									
PCT. SPAN	90	70	50	30	10	UBAR	0.0012	0.0005	-0.0071	0.0167	0.1327	DFAC	0.4320	0.4305	0.4300	0.4583	0.6038		
BETA 2	54.097	55.103	55.608	55.757	59.122	EFFP	0.4150	0.4604	0.4604	0.4919	0.6449	EFF	1.2161	1.4663	1.8114	1.3925	1.1361		
BETA 3	23.179	24.267	24.267	24.267	24.267	INCLD	1.2220	1.4803	1.4274	1.4050	1.1406	INCLD	3.97	1.16	0.58	0.5258	0.5424		
V 2	738.81	748.53	740.67	730.43	711.79	DEV	8.6226	6.831	6.890	7.244	7.564	U 2	623.63	650.43	677.84	705.25	732.67		
V2 2	398.49	491.76	528.80	549.34	499.30	M(PK) 1	0.5015	0.4998	0.4933	0.4581	0.4130	M(PK) 2	0.6764	0.6874	0.6784	0.6676	0.6449		
V2 2A	357.02	428.24	418.37	411.01	365.30	TURN(PR)	31.561	31.930	30.159	29.066	29.081	U 2	623.63	650.43	677.84	705.25	732.67		
V-THETA 2	598.44	611.93	611.93	603.81	610.91	U 1	0.5015	0.4998	0.4933	0.4581	0.4130	V 2	623.63	650.43	677.84	705.25	732.67		
V-THETA 2A	177.01	201.28	176.04	216.22	205.21	V 1	0.5015	0.4998	0.4933	0.4581	0.4130	V 2	623.63	650.43	677.84	705.25	732.67		
M 2	0.6764	0.6874	0.6784	0.6676	0.6449	V 1	0.5015	0.4998	0.4933	0.4581	0.4130	V 2	623.63	650.43	677.84	705.25	732.67		
M 2A	0.3503	0.4420	0.4693	0.4489	0.4407	V 1	0.5015	0.4998	0.4933	0.4581	0.4130	V 2	623.63	650.43	677.84	705.25	732.67		
TURN	27.725	31.252	31.163	32.578	34.855	V 1	0.5015	0.4998	0.4933	0.4581	0.4130	V 2	623.63	650.43	677.84	705.25	732.67		

	DFAC	EFFP	INCID	LOSS PARA	DEV	OLY
0.6986	0.5755	0.5534	0.4996	0.5796		
0.4702	0.5161	0.5157	0.5279	0.4750		
-3.60	-2.60	-2.09	-1.94	1.44		
1.1995	0.0264	.0748	.0610	.0485		
27.01	24.49	20.09	23.82	24.91		
21.64	21.00	21.00	22.00	20.00		

Table B-2. Blade Element Performance (Continued)

PERCENT DESIGN SPEED = 109.98

CORRECTED WEIGHT FLOW = 89.00

CORRECTED ROTOR SPEED = 4234.06

INLET GUIDE VANE		STATION 0 - STATION 1						STATION 1 - STATION 2						FLOW GENERATOR ROTOR					
PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10	PCT. SPAN	90	70	50	30	10		
DIA	33.622	35.167	36.711	38.256	39.801	DIA	33.589	35.067	36.545	38.023	39.501	UUBAR	0.5524	0.5158	0.5110	0.4707	0.5312		
BETA 0	0.000	0.000	0.000	0.000	0.000	BETIA 1	34.800	36.800	37.600	37.200	36.300	BETIA 2	0.5585	0.5322	0.5612	0.4966	0.4925		
BETA 1	34.800	36.800	37.600	37.200	36.900	BETIA 1	52.603	53.435	53.921	54.088	56.423	BETIA 2	-5.10	-4.26	-3.78	-3.61	-1.28		
V 0	382.84	382.84	382.84	382.84	382.84	BETA(PR) 1	30.311	32.453	35.508	38.835	43.805	BETA(PR) 2	0.07908	0.07120	0.06617	0.05857	0.1074		
V 1	591.14	596.25	577.00	567.31	537.72	BETIA(PR) 2	2.136	4.009	8.408	12.393	17.974	V 1	591.14	589.25	577.00	567.31	537.72		
VZ 0	382.84	382.84	382.84	382.84	382.84	V 1	591.14	589.25	577.00	567.31	537.72	VZ 1	748.25	746.74	748.25	740.71	720.71		
VZ 1	485.42	469.43	457.15	451.88	430.01	VZ 2	759.45	757.15	757.15	751.88	730.01	VZ 1	485.42	469.43	469.43	451.88	430.01		
V-THETA 0	0.00	0.00	0.00	0.00	0.00	VZ 2	485.42	469.43	469.43	451.88	430.01	V-THETA 1	351.17	342.86	342.86	341.24	348.88		
V-THETA 1	337.37	351.17	352.05	342.99	322.86	V-THETA 1	337.37	337.37	351.17	352.05	342.99	V-THETA 2	0.3470	0.3470	0.3470	0.3470	0.3470		
M 0	0.3470	0.3470	0.3470	0.3470	0.3470	V-THETA 2	603.34	615.83	609.51	606.02	600.46	V(PK) 1	562.3	556.3	561.6	580.1	595.8		
M 1	0.5451	0.5403	0.5313	0.5219	0.5219	V(PK) 1	461.6	457.9	448.9	449.3	449.0	V(PK) 2	0.2307	0.2307	0.2307	0.2307	0.2307		
TURN	-34.80	-36.80	-37.60	-37.20	-36.90	V(PK) 2	-283.8	-283.8	-283.8	-283.8	-283.8	VTHETA PR1	-17.2	-32.0	-65.6	-96.4	-142.4		
UUBAR	C.0324	0.0128	0.0315	0.0528	0.0528	VTHETA PR1	621.16	649.69	678.23	706.76	735.30	VTHETA PR2	603.34	615.83	615.83	615.83	615.83		
DFAC	-0.119	-0.061	-0.034	-0.016	0.039	VTHETA PR2	620.54	647.85	675.15	702.46	729.76	U 1	0.5451	0.5403	0.5313	0.5219	0.4933		
EFFP	0.9842	0.9770	0.9835	0.9667	0.8235	U 2	0.5451	0.5403	0.5313	0.5219	0.4933	U 1	0.6984	0.7072	0.6937	0.6779	0.6555		
INCID	*****	26.9001	27.3001	27.7001	28.0001	U 2	0.5451	0.5403	0.5313	0.5219	0.4933	M 1	0.5171	0.5336	0.5466	0.5336	0.5171		
DEV	7.300	6.100	6.100	7.700	8.400	M 2	0.5171	0.5223	0.4130	0.4083	0.3811	M (PR) 1	0.4244	0.4244	0.4244	0.4244	0.4244		
SLOTTED STATOR 3		STATION 2 - STATION 2A						STATION 2 - STATION 2A						STATION 2 - STATION 2A					
PCT. SPAN	90	70	50	30	10	UUBAR	0.0351	-0.0409	-0.0490	-0.0490	-0.0490	EFF	1.2497	1.5426	1.4998	0.9826	1.1817		
BETA 2	52.603	53.435	53.921	54.088	56.423	EFF	-1.13	-3.19	-3.19	-3.19	-3.19	INCID	0.2305	0.2305	0.2305	0.2305	-1.55		
BETA 3	26.378	22.158	22.333	22.880	26.013	INCID	-1.13	-3.19	-3.19	-3.19	-3.19	DEV	7.5116	5.969	6.248	5.773	7.104		
V 2	759.45	756.74	754.15	748.25	720.71	DEV	0.3767	0.3678	0.3678	0.3678	0.3678	EFFAC	1.2435	1.5214	1.4856	0.9831	1.1763		
V 2A	499.11	549.45	565.24	571.05	521.13	EFFAC	0.5185	0.5127	0.5127	0.5127	0.5127	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		
VZ 2	461.24	456.78	444.12	438.88	398.59	UUBAR	0.4244	0.4244	0.4244	0.4244	0.4244	TURN(PR)	28.176	28.444	27.099	26.442	25.832		
VZ 2A	447.15	503.87	536.55	531.65	468.10	TURN(PR)	603.34	615.83	609.51	606.02	600.46	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074		
V-THETA 2	603.34	615.83	609.51	606.02	596.46	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		
V-THETA 3	221.75	207.23	177.79	224.36	229.05	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074		
M 2	0.6984	0.7012	0.6937	0.6799	0.6555	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		
M 2A	C.4439	0.4974	0.5064	0.5172	0.4634	UUBAR	0.07908	0.07120	0.06617	0.05857	0.1074	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		
TURN	26.225	31.277	35.598	31.208	30.350	UUBAR	0.2103	0.1757	0.1532	0.1347	0.2460	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		
DIA	33.564	34.992	36.420	37.848	39.276	UUBAR	0.2103	0.1757	0.1532	0.1347	0.2460	UUBAR	0.5524	0.5322	0.5223	0.4223	0.3811		

APPENDIX C
REFERENCES

1. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part I - Analysis and Design," NASA CR-54544, PWA FR-1713, July 1966.
2. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part II - Annular Cascade Investigation of Slot Location and Geometry," NASA CR-54545, PWA FR-1669, September 1966.
3. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part III - Data and Performance for Slotted Rotor 1," NASA CR-54546, PWA FR-2110, February 1967.
4. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part IV - Data and Performance for Slotted Rotor 2," NASA CR-54547, PWA FR-2111, February 1967.
5. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part V - Data and Performance for Slotted Rotor 3," NASA CR-54548, PWA FR-2285, August 1967.
6. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part VI - Data and Performance for Slotted Stator 1," NASA CR-54549, PWA FR-2286, August 1967.
7. "Single Stage Experimental Evaluation of Slotted Rotor and Stator Blading, Part VII - Data and Performance for Slotted Stator 2," NASA CR-54550, PWA FR-2287, September 1967.
8. Aerodynamic Design of Axial Flow Compressors (Revised), NASA SP-36, 1965, p 248.

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